



CPT Interpretation - Soil Type

Peter K. Robertson

CPT in Geotechnical Practice

Santiago, Chile

July, 2014



GUIDE TO CONE PENETRATION TESTING



*Robertson
& Cabal (Robertson)*



*5th Edition
2012*

CPT Guide 5th Edition

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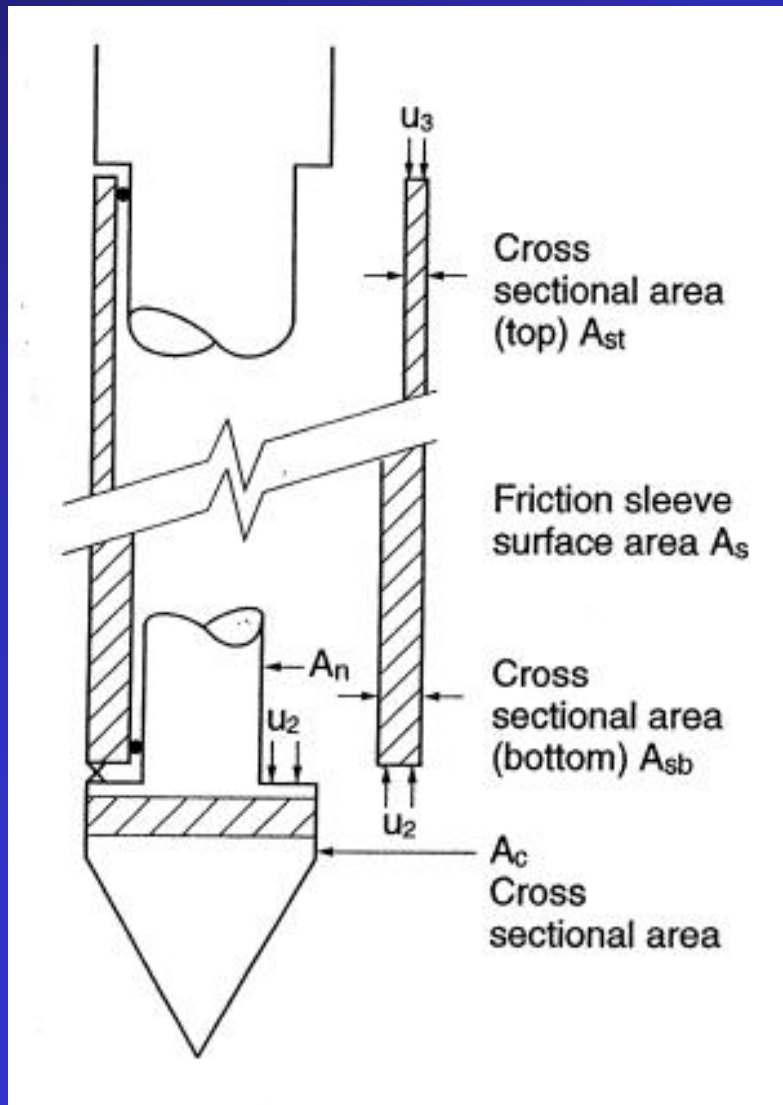
Webinars

Recordings of previous webinars are available on YouTube: search for '*CPT Robertson*' or

<http://www.youtube.com/watch?v=alrzeelWpZc>



Unequal End Area Effects on q_c



$$q_t = q_c + u_2(1-a)$$

$$a = 0.60 \text{ to } 0.85$$

a = tip net area ratio
 $\sim A_n/A_c$

In sands: $q_t = q_c$

In very soft clays:
correction to q_t is important

Cones should have high net area ratio
 $a > 0.8$

Role of CPT

CPT has three main applications:

- Determine sub-surface stratigraphy and identify materials present (*Soil Type – SBT*)
- Estimate soil parameters
- Provide results for direct geotechnical design

Primary role is soil profiling and can be supplemented by samples, other in-situ tests and laboratory testing

CPTu Interpretation

Soil Type

- Soil behavior type (*SBT*) & stratigraphy

In-situ State

- Relative density (D_r) or State Parameter (ψ) and *OCR*

Strength

- Peak friction angle (ϕ') and undrained strength (s_u)

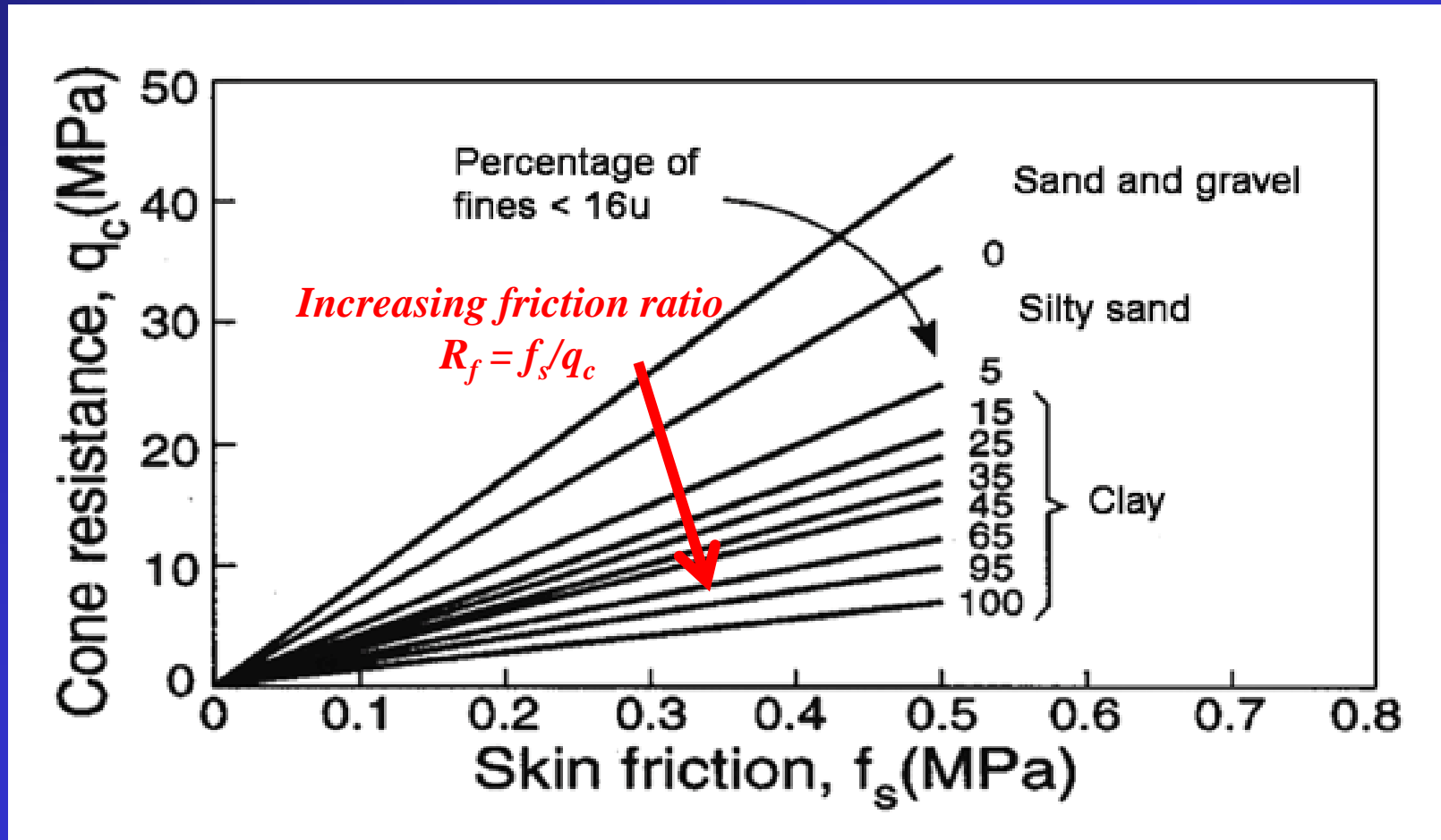
Stiffness/compressibility

- Shear (G_o), Young's (E') and 1-D constrained (M)

Consolidation/permeability

- Coeff of consolidation (c_v) and permeability (k)

First CPT 'soil classification' chart

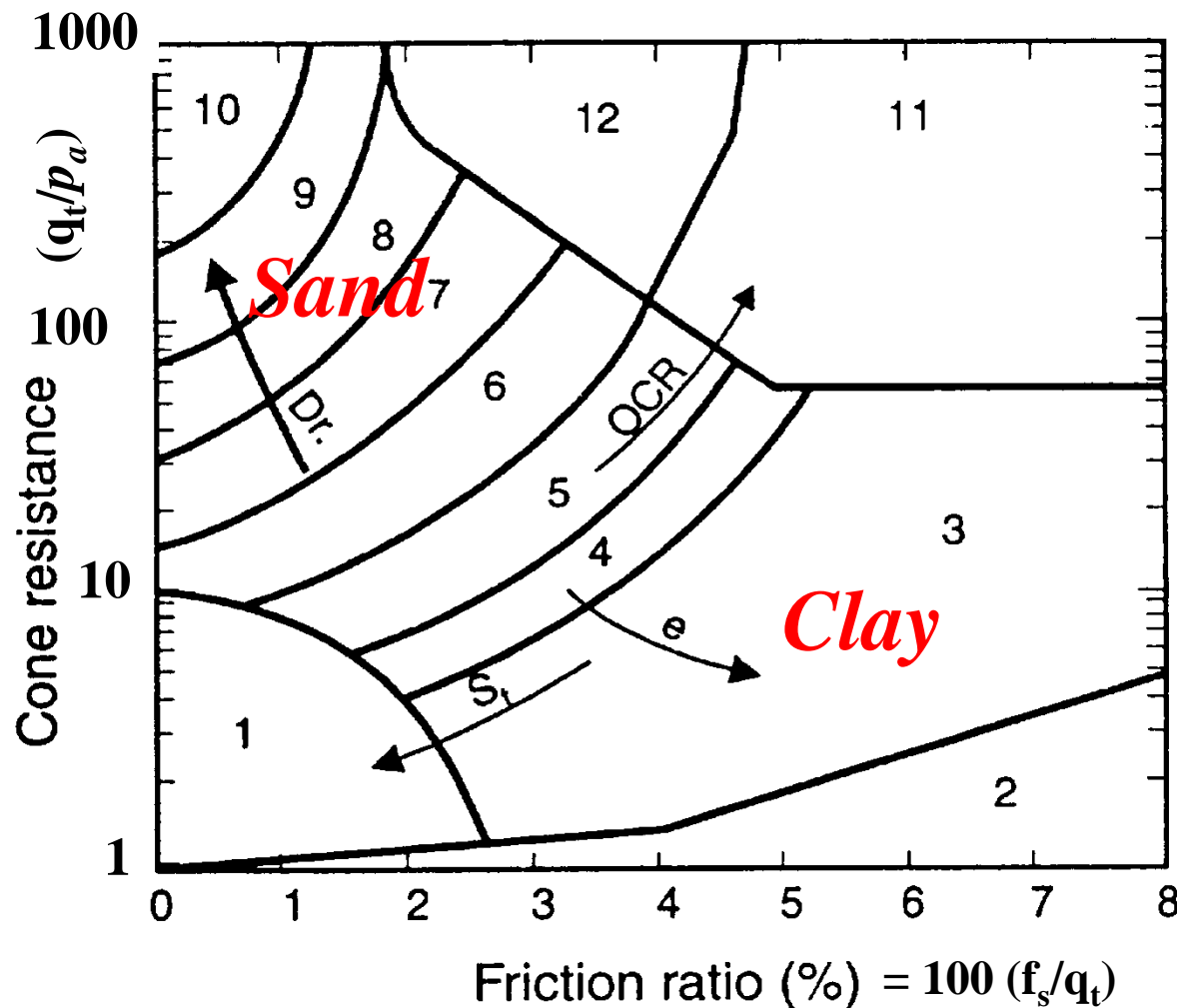


Begemann (1965) type mechanical cone

CPT-based “classification”

- CPT measurements are influenced by *in-situ behavioral characteristics*, such as strength, stiffness and compressibility. These characteristics are controlled primarily by soil state, in-situ effective stresses, stress history, age, and cementation, as well as mineralogy.
- Traditional soil classification systems are based on *physical characteristics* obtained on *remolded samples*, such as grain size, fines content and plasticity. These characteristics are controlled primarily by depositional environment and geology.

Soil Behaviour Type (SBT) Chart



Zone	Soil behaviour type
1	Sensitive fine grained
2	Organic material
3	Clay
4	Silty Clay to clay
5	Clayey silt to silty clay
6	Sandy silt to clayey silt
7	Silty sand to sandy silt
8	Sand to silty sand
9	Sand
10	Gravelly sand to sand
11	Very stiff fine grained*
12	Sand to clayey sand*

* Overconsolidated or cemented

SBT

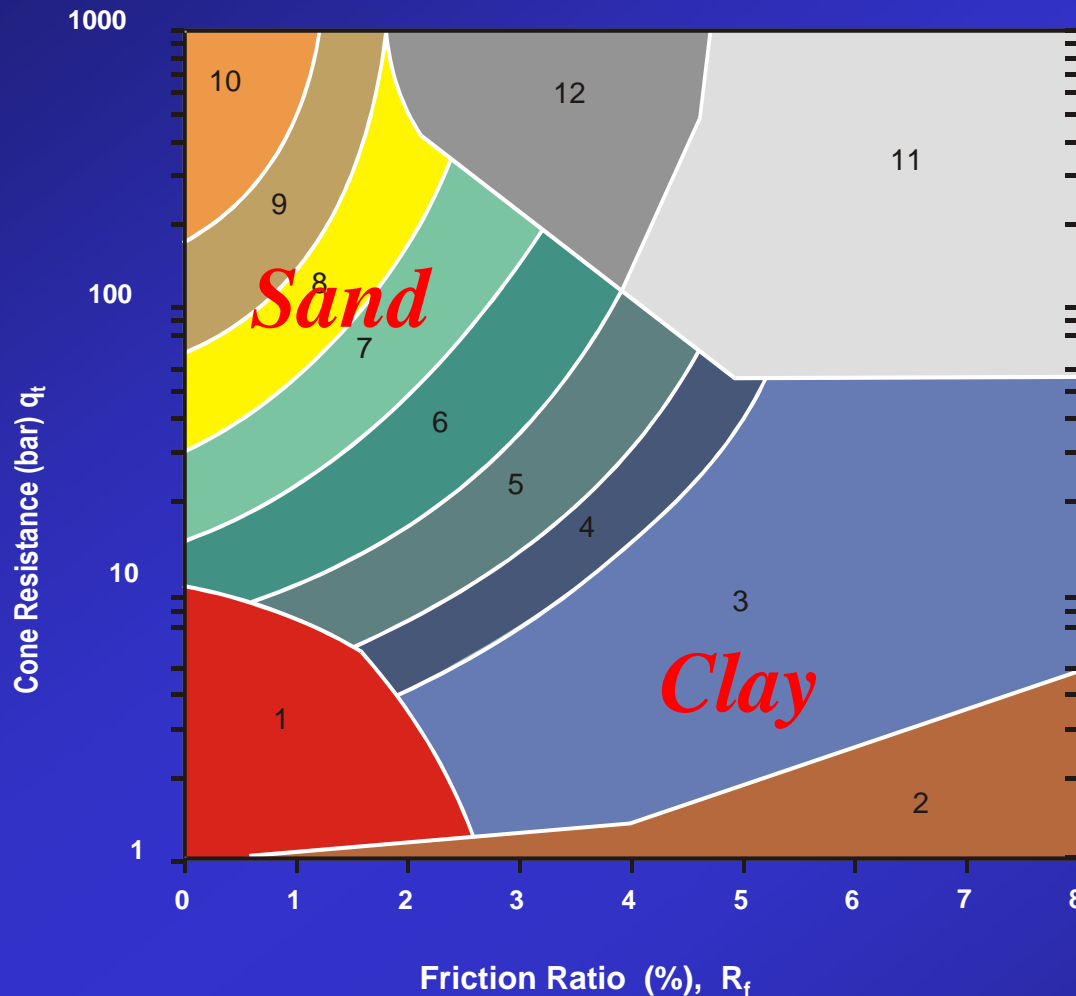
Robertson & Campanella, 1986

Note: 1 tsf ~ 0.1 MPa

Robertson, 2014

CPT - Soil Behavior Type (SBT)

Non-Normalized Classification Chart



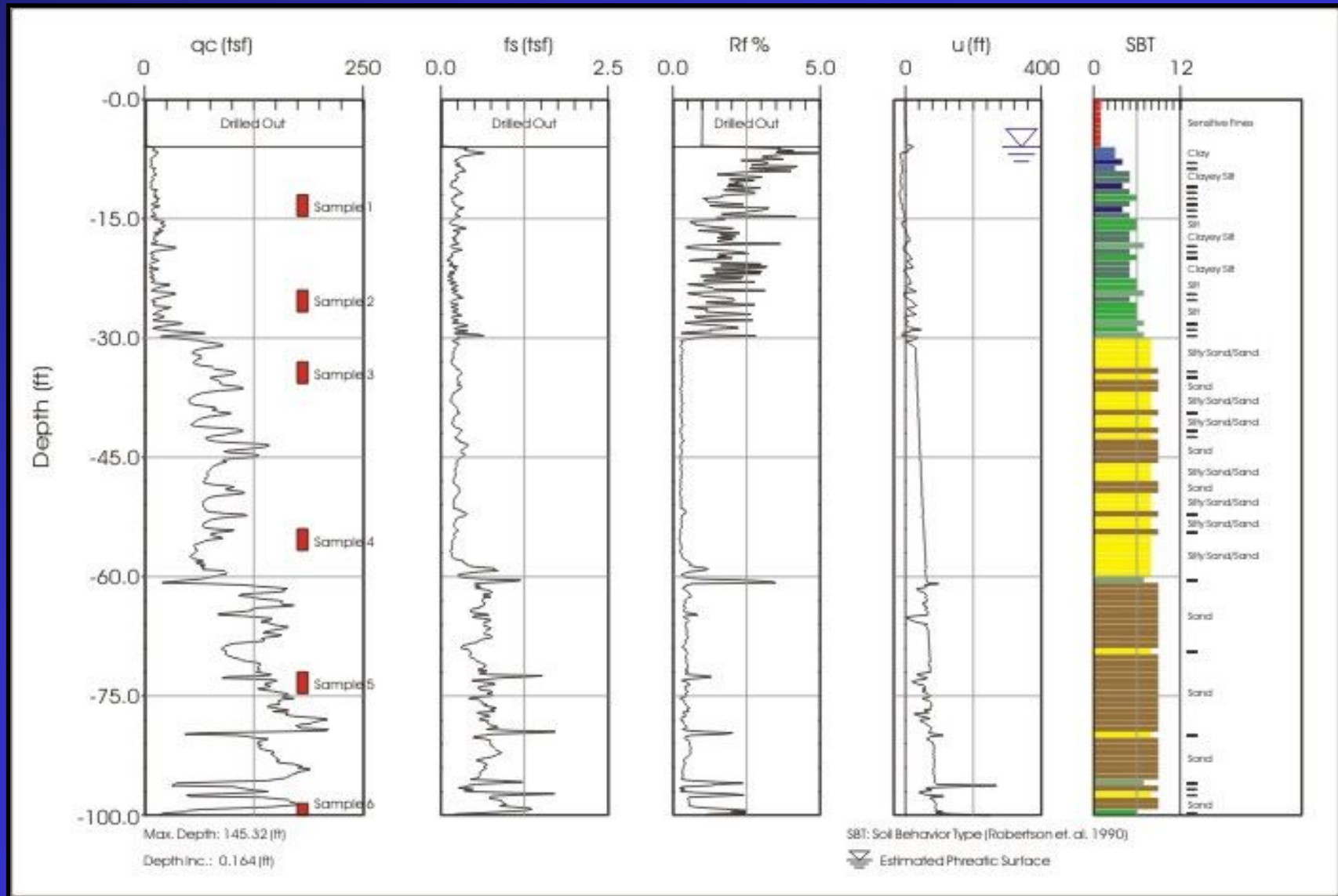
CPT SBT based on in-situ soil behavior (strength, stiffness, compressibility) - not the same as classification based Atterberg Limits and grain size carried out on disturbed samples

Robertson & Campanella, 1986

Note: 1 bar ~ 1 tsf ~ 0.1 MPa

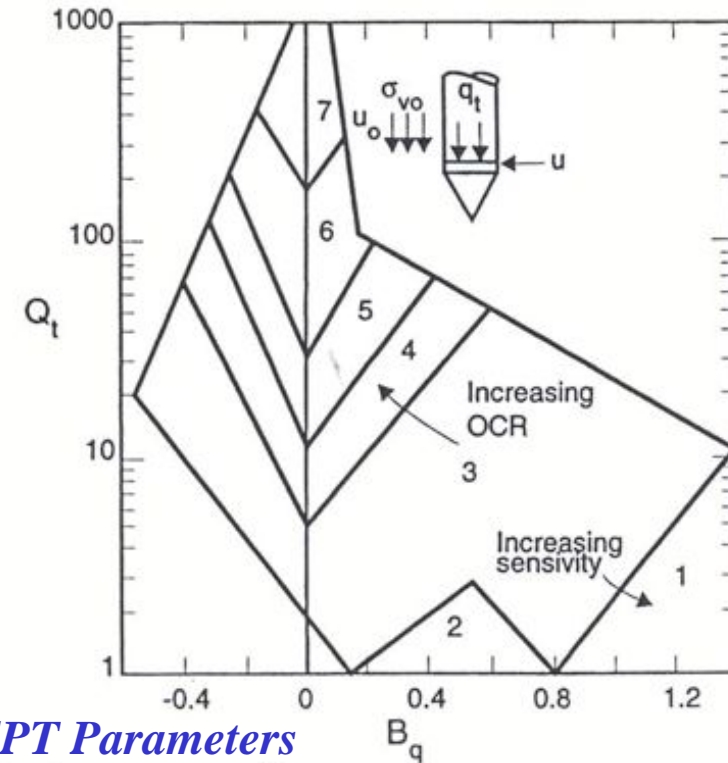
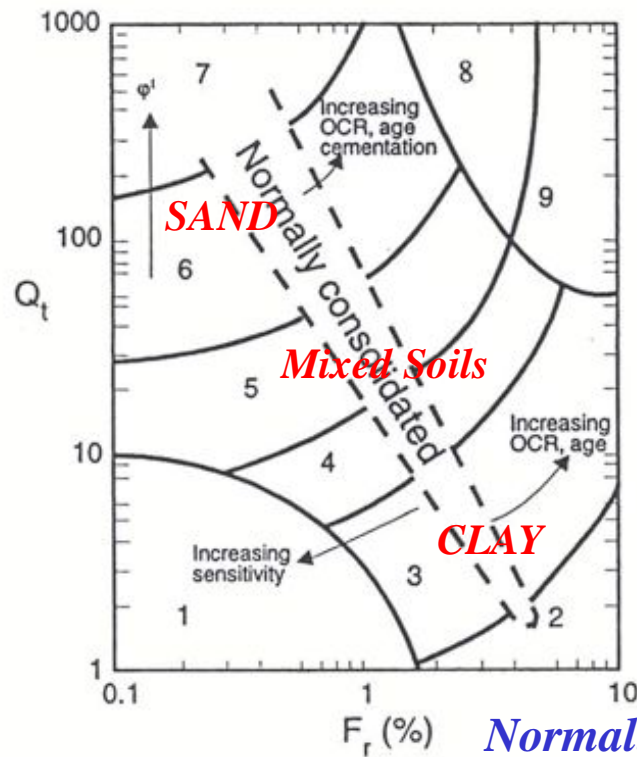
Robertson, 2014

CPT Data Presentation



Example CPTu Plot

Normalized SBTn Charts



Normalized CPT Parameters

$$Q_t = \frac{q_t - \sigma_{vo}}{\sigma'_{vo}}$$

$$B_q = \frac{u_2 - u_o}{q_t - \sigma_{vo}}$$

$$F_r = \frac{f_s}{q_t - \sigma_{vo}} \times 100\%$$

Robertson, 1990

Zone Soil behaviour type

1. Sensitive, fine grained;
2. Organic soils-peats;
3. Clays-clay to silty clay;

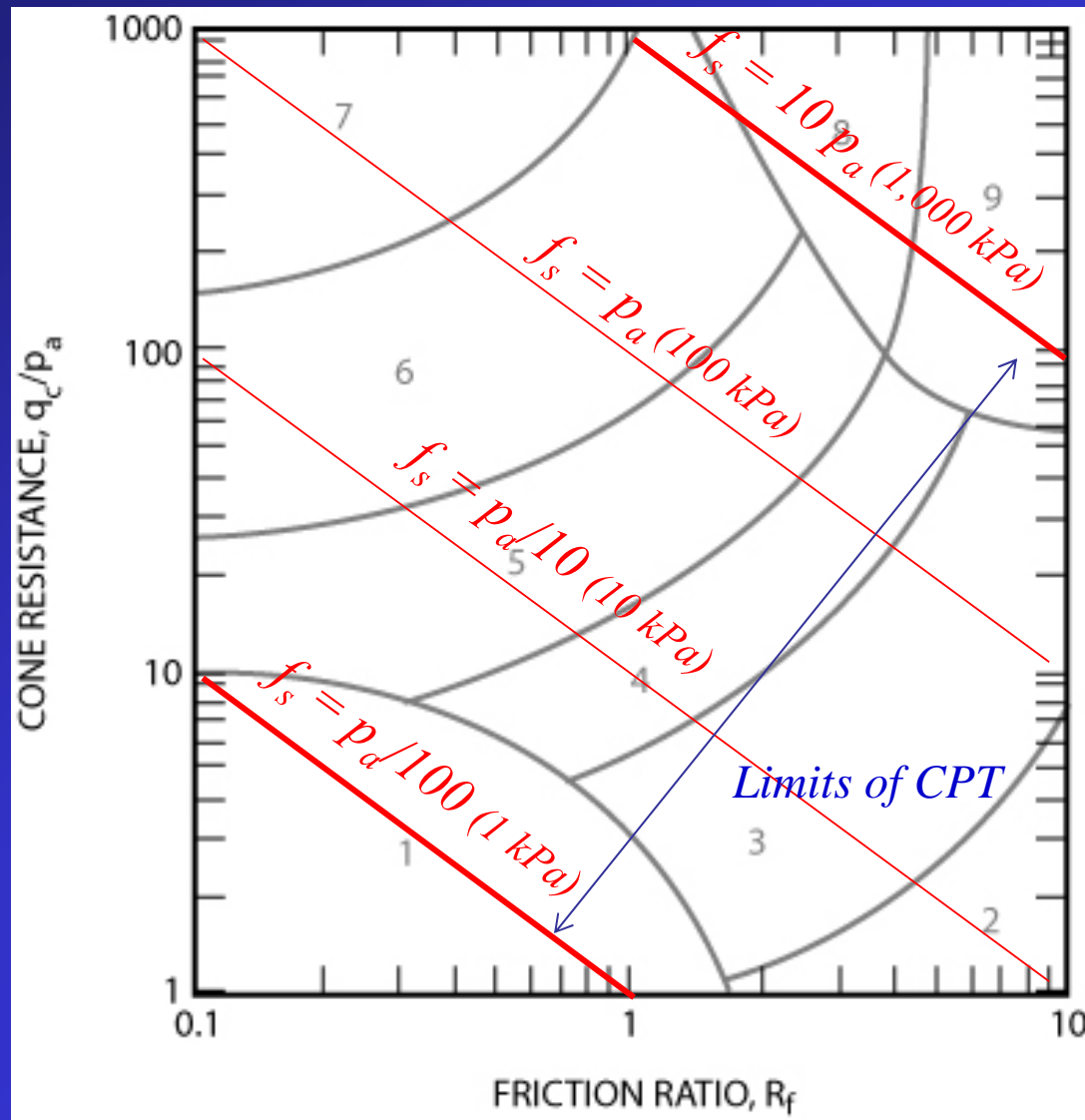
Zone Soil behaviour type

4. Silt mixtures clayey silt to silty clay
5. Sand mixtures; silty sand to sand silty
6. Sands; clean sands to silty sands

Zone Soil behaviour type

7. Gravely sand to sand;
8. Very stiff sand to clayey sand
9. Very stiff fine grained

Dimensionless SBT chart



In 2010 Robertson (CPT' 10) updated the SBT chart to use dimensionless parameters and to simplify the chart to 9 zones to be consistent with the normalized SBT chart (Robertson, 1990)

p_a = atmospheric pressure = 100 kPa = 1 tsf

Proposed common SBT zones

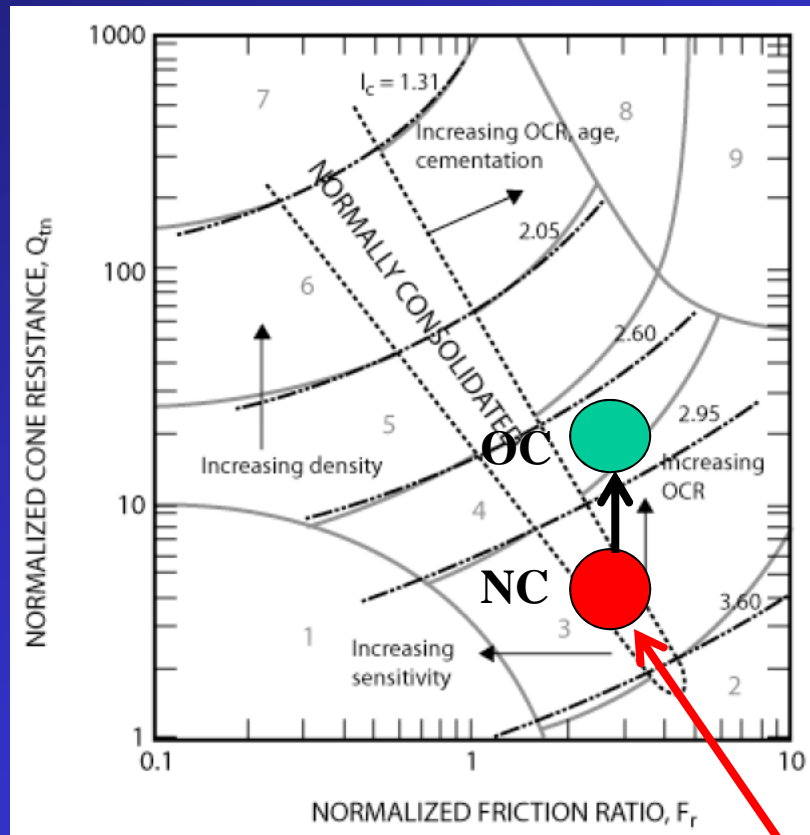
SBT zone Robertson et al (1986)	SBTn zone Robertson (1990)	Proposed common SBT description
1	1	Sensitive fine-grained
2	2	Clay: organic soil
3	3	Clays: clay to silty clay
4 & 5	4	Silt mixtures: clayey silt & silty clay
6 & 7	5	Sand mixtures: silty sand to sandy silt
8	6	Sands: clean sand to silty sand
9 & 10	7	Dense sand to gravelly sand
12	8	Stiff sand to clayey sand*
11	9	Stiff fine-grained*

Robertson, 2010

Robertson, 2014

Why Friction Ratio (f_s/q_t)?

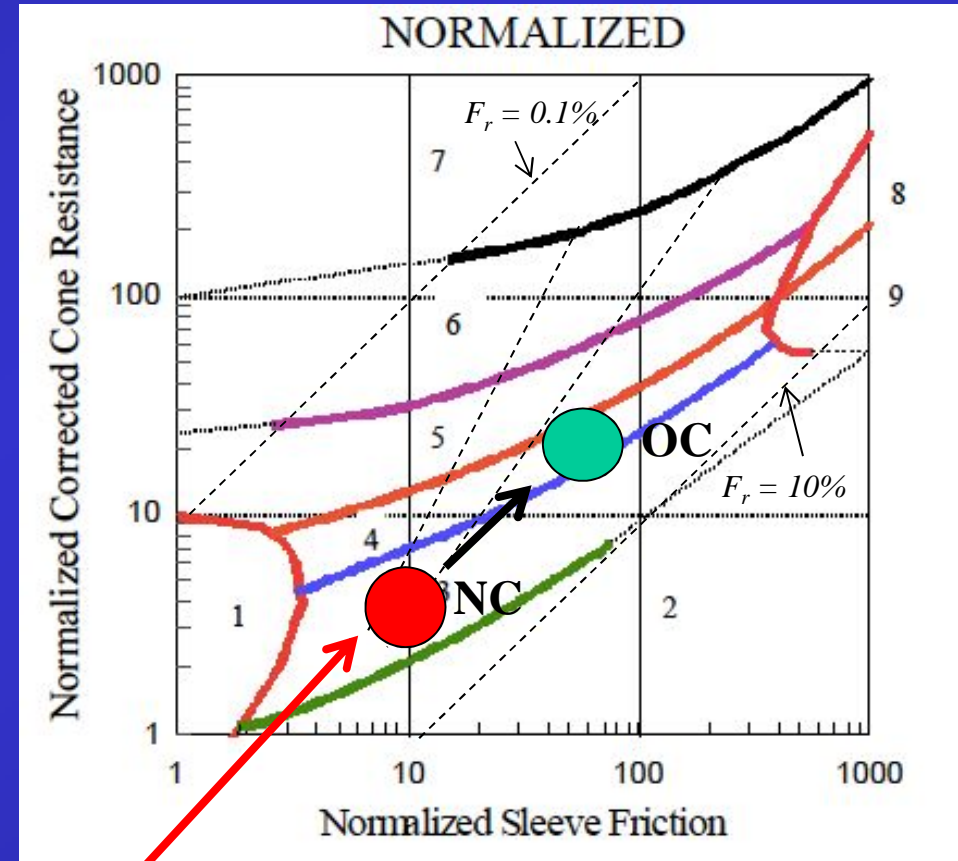
$$Q_t = (q_t - \sigma'_{vo}) / \sigma'_{vo}$$



$$F_r = 100[f_s / (q_t - \sigma'_{vo})]$$

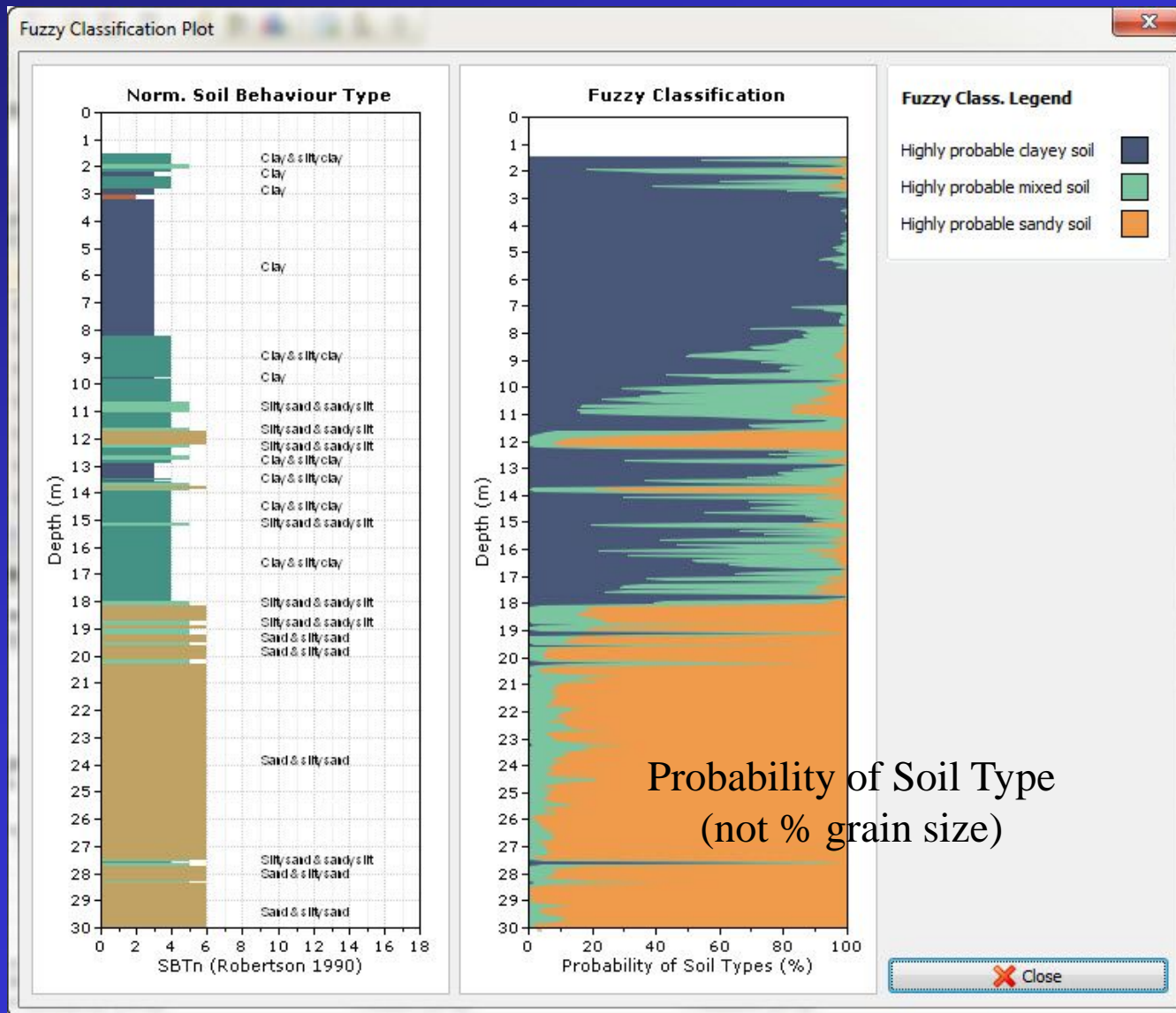
Normally to OC consolidated clay, friction ratio, $F_r \sim \text{constant}$

$$Q_t = (q_t - \sigma'_{vo}) / \sigma'_{vo}$$



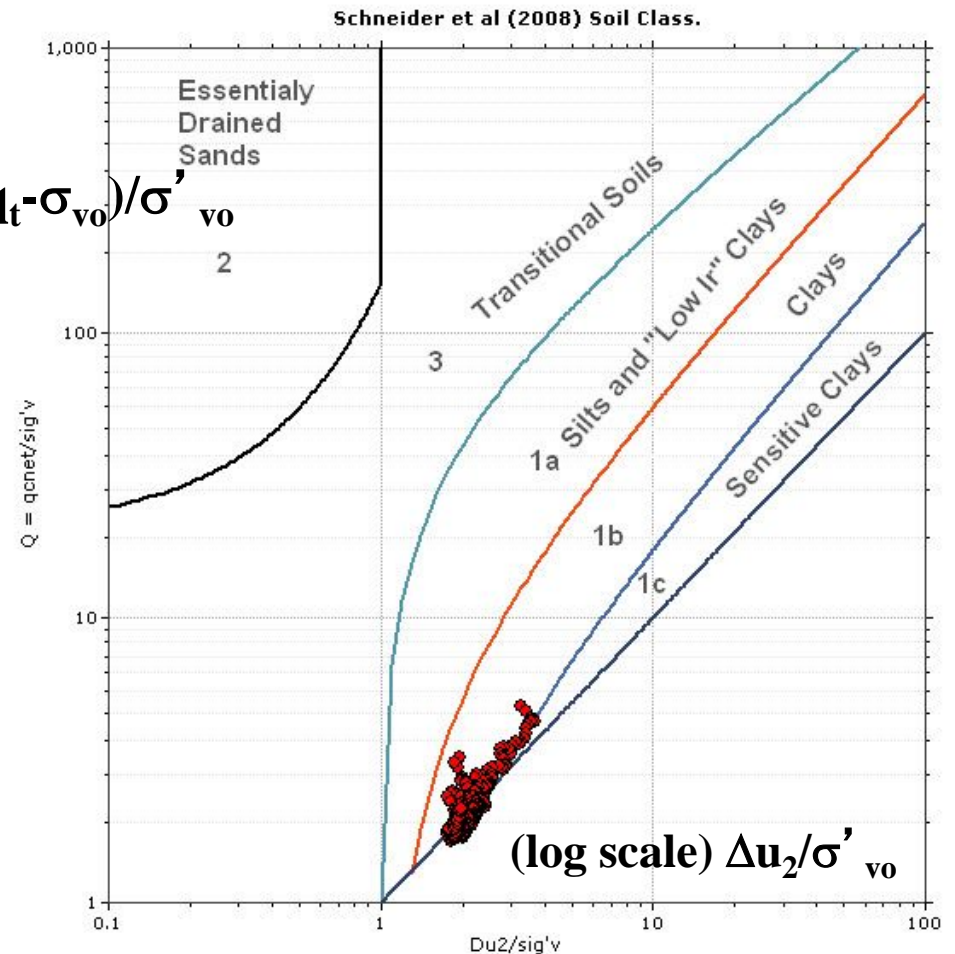
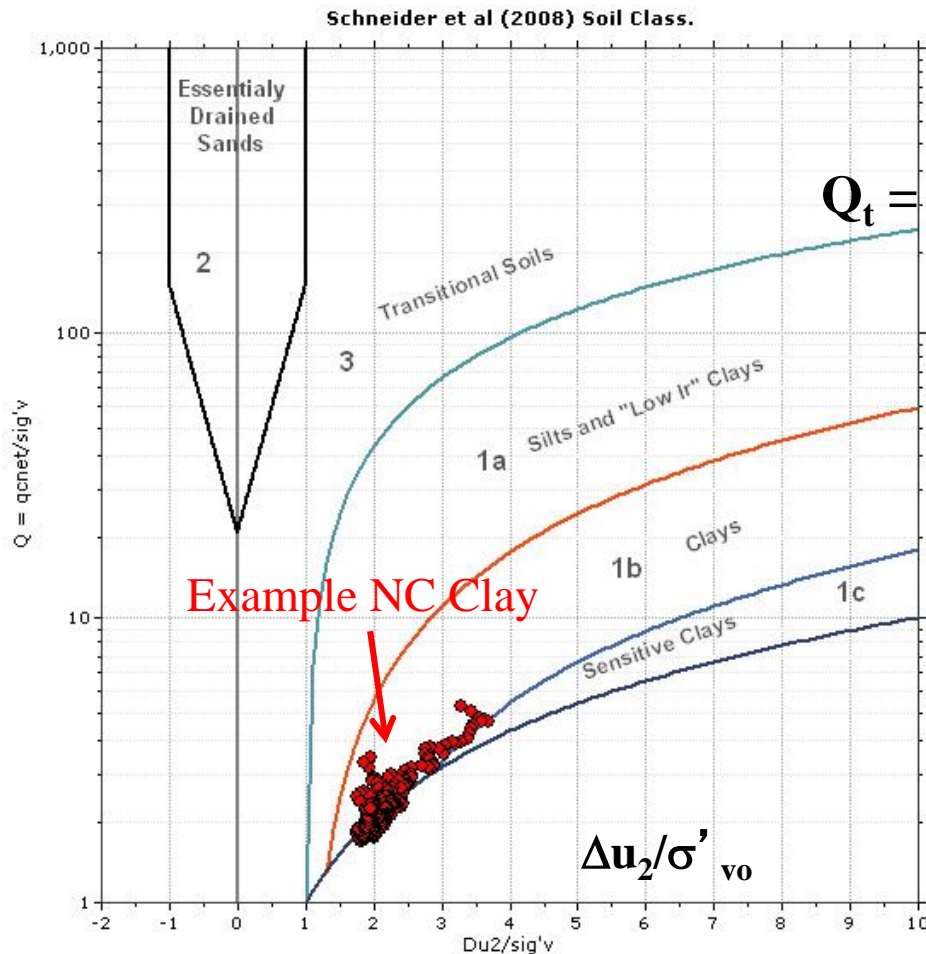
$$F = 100(f_s / \sigma'_{vo})$$

Tumay Fuzzy-logic SBT



*Applies
fuzzy
logic to
SBT*

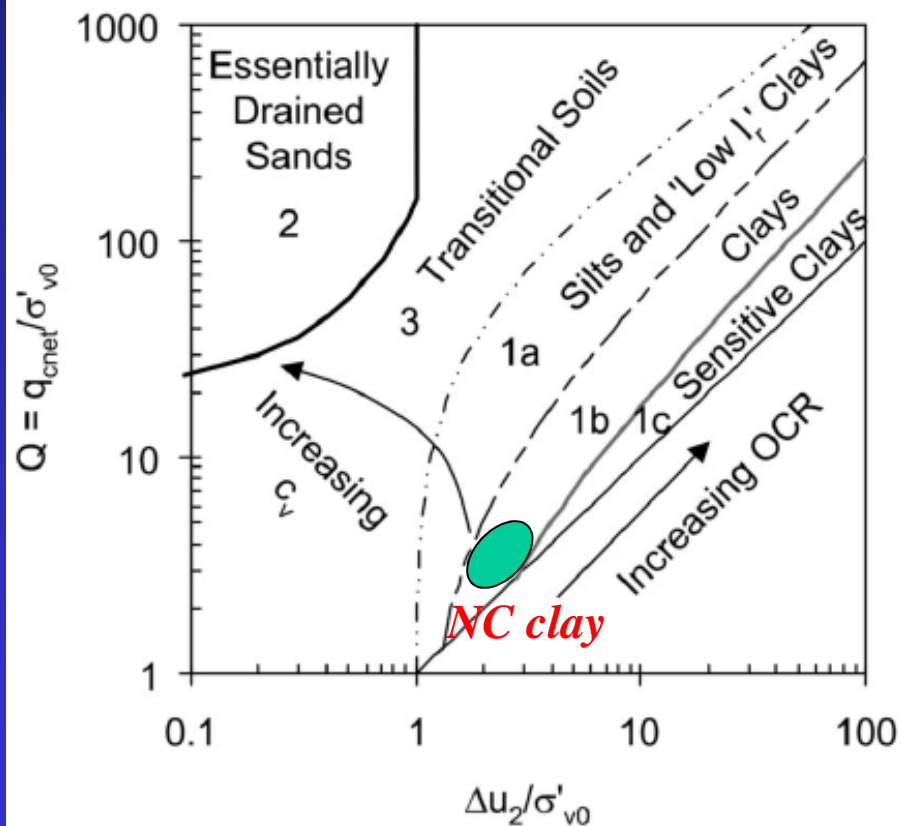
Schneider et al (2008) chart



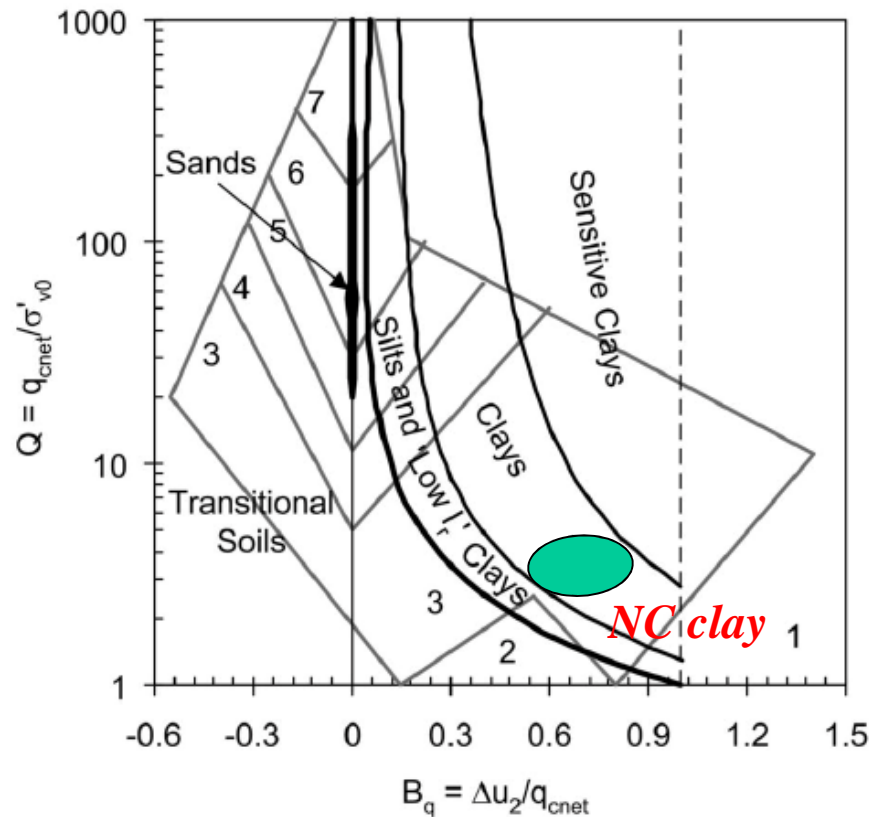
Combines normalized cone resistance (Q) and excess pore pressure ($\Delta u/\sigma'_{\text{v}}$)
 Good offshore – less effective on-shore, where saturation can not be assured

Robertson, 2014

Compare pore pressure charts

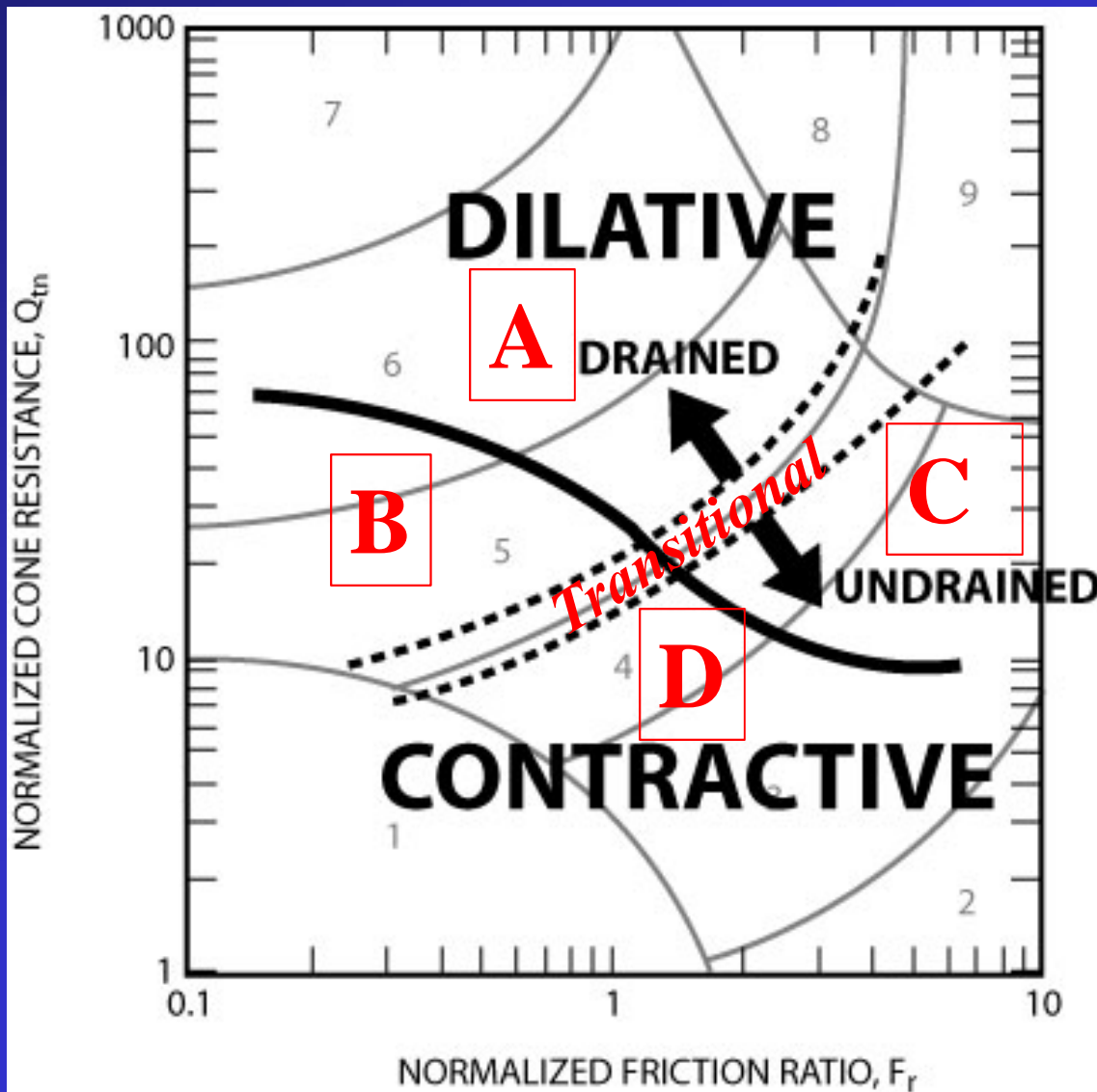


Schneider et al, 2008



Modified Robertson (1990)

Generalized CPT Soil Behaviour Type



CPT Soil Behaviour

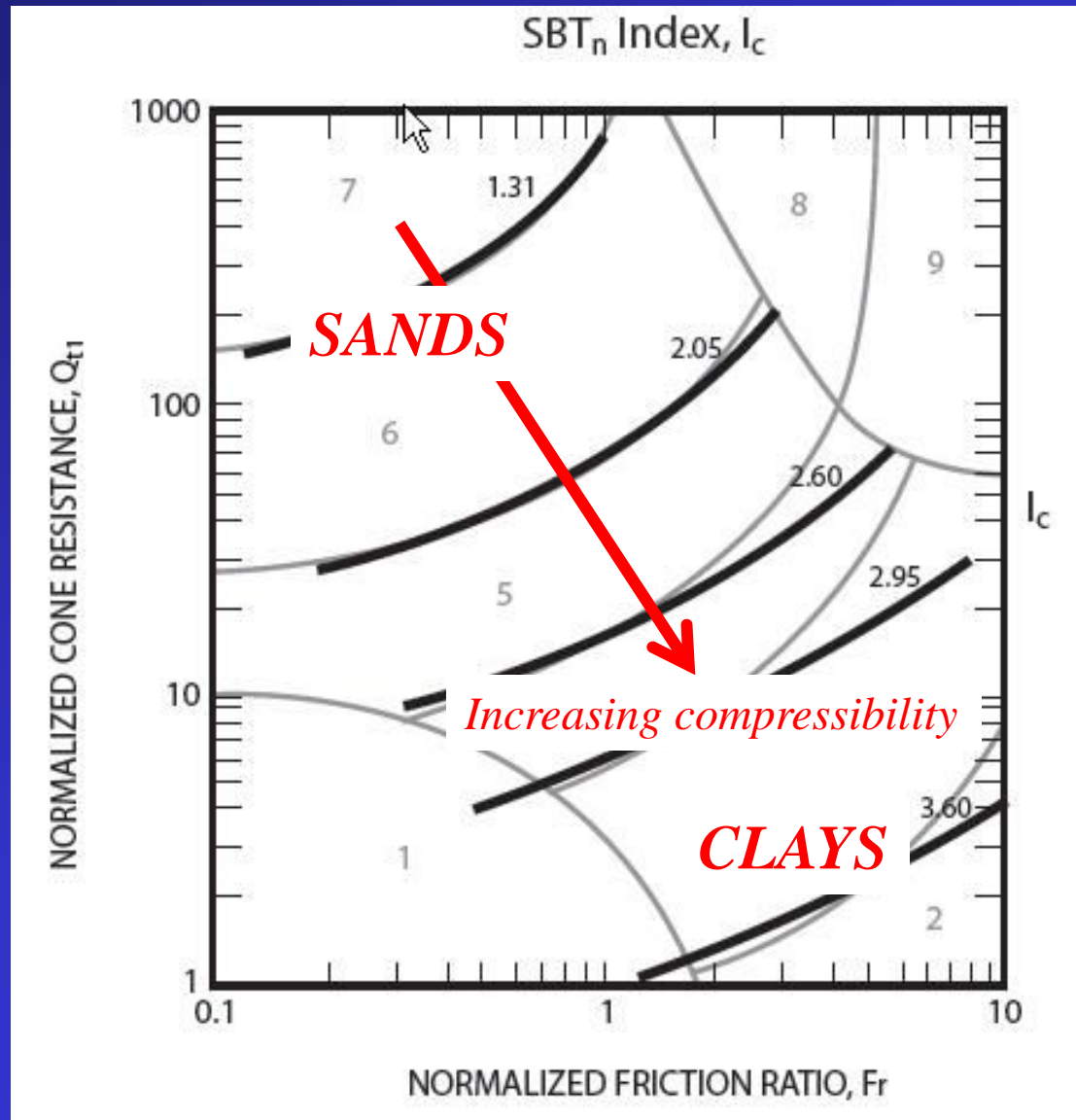
A: Coarse-grain-dilative

B: Coarse-grain-contractive

C: Fine-grain-dilative

D: Fine-grain-contractive

CPT SBT Index, I_c



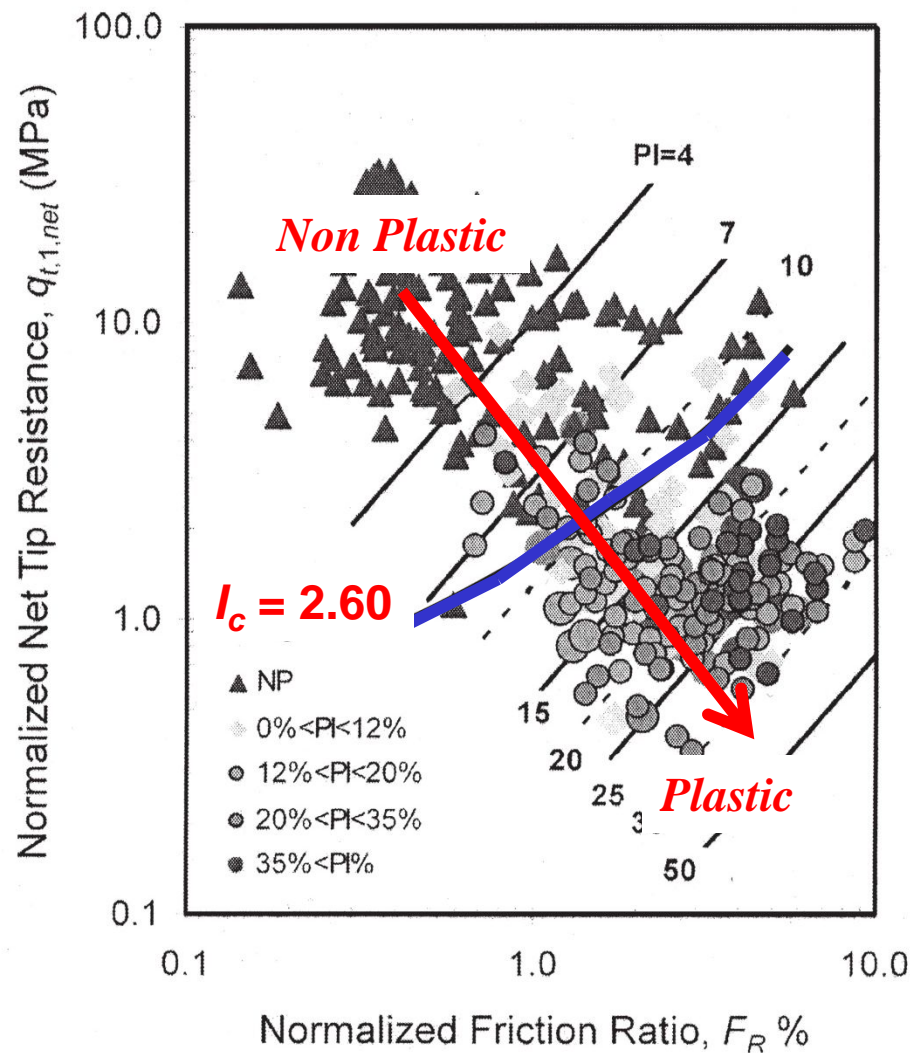
*Soil Behavior Type
Index, I_c*

$$I_c = [(3.47 - \log Q)^2 + (\log F + 1.22)^2]^{0.5}$$

**Function primarily of
Soil Compressibility**

*$I_c > 2.60$ predominately
fine grained 'clay-like' soil*

SBT from CPT



Plasticity Index as
function of SBT I_c

Boundary between
sand-like and *clay-like*
soils is $PI \sim 10$

When $I_c < 2.60$
95% samples NP
84% with $PI < 12\%$

Data from Cetin & Ozan, 2009

CPT Normalization

- Early normalization based on theory for clays

$$Q_t = (q_t - \sigma_v) / \sigma'_v$$

- Recently normalization based on soil type, density and stress level

$$Q_{tn} = [(q_t - \sigma_v)/p_a] (p_a/\sigma'_v)^n$$

Where:

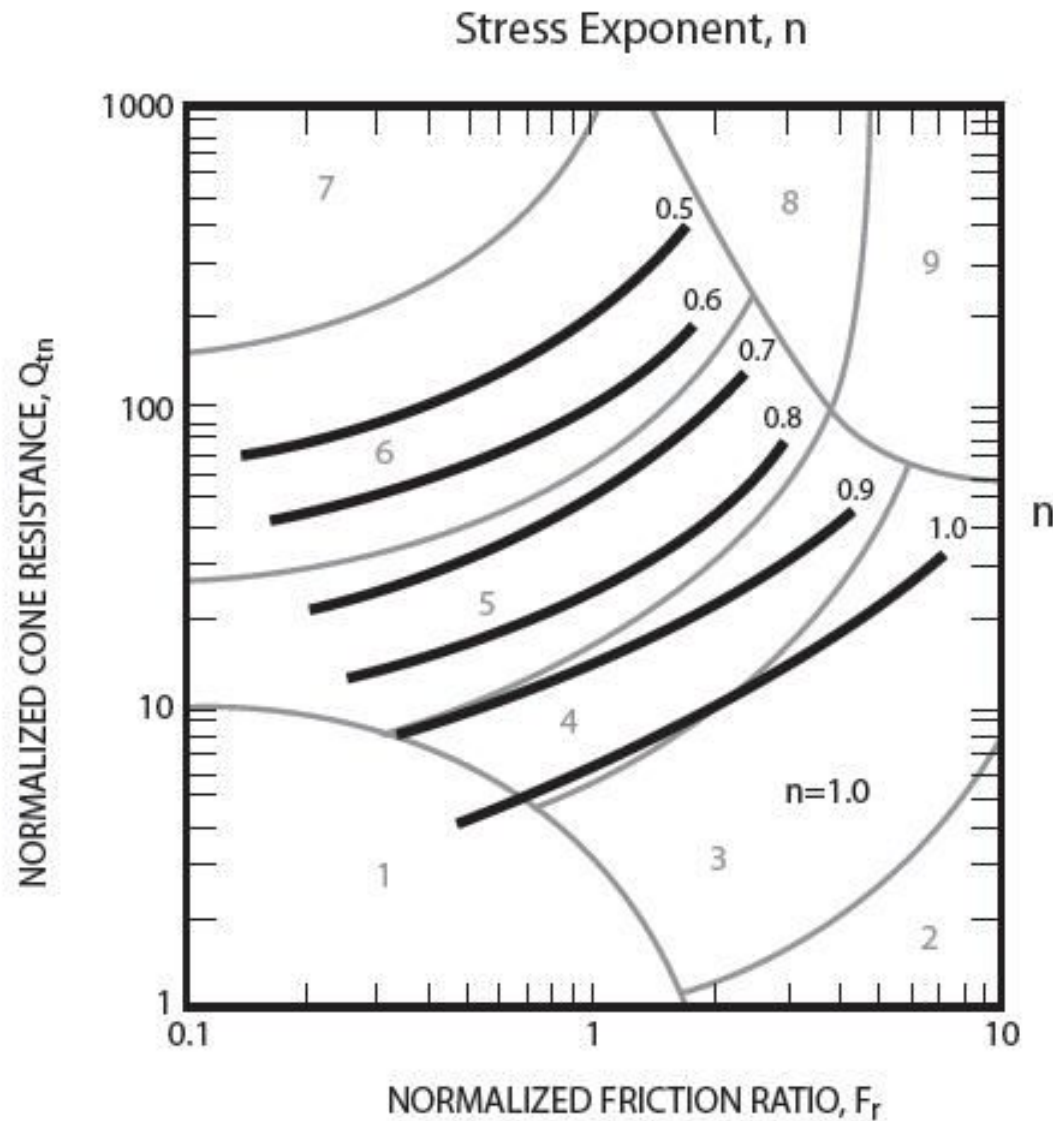
$(q_t - \sigma_v)/p_a$ = dimensionless net cone resistance,

$(p_a/\sigma'_v)^n$ = stress normalization factor

n = stress exponent that varies with soil type, density & stress level

p_a = atmospheric pressure in same units as q_t and σ_v

CPT Normalization



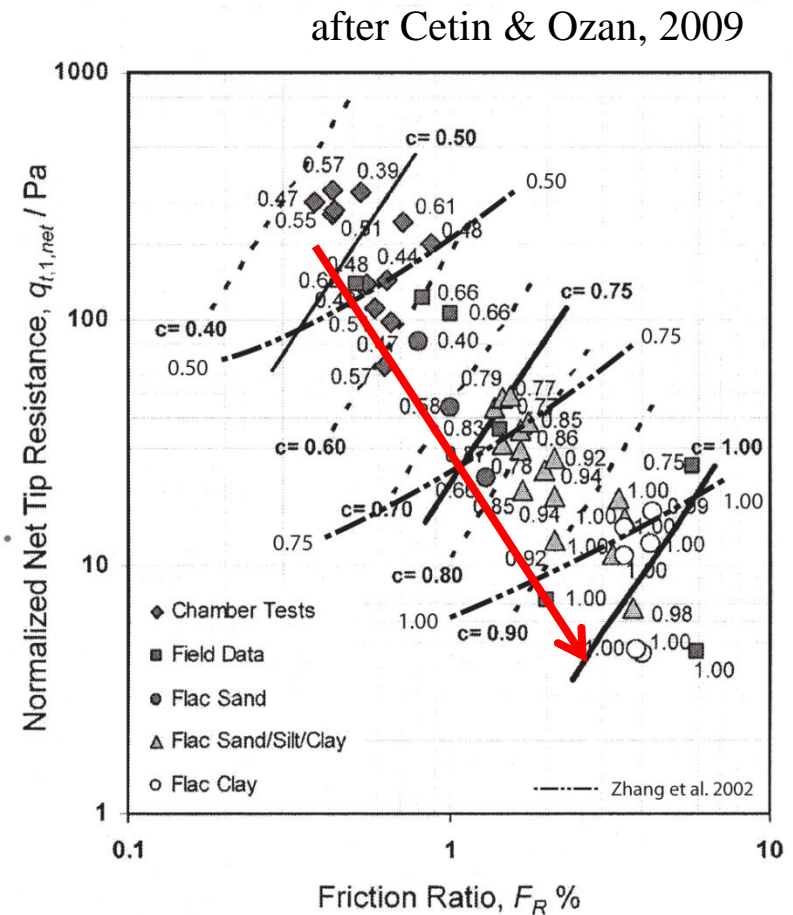
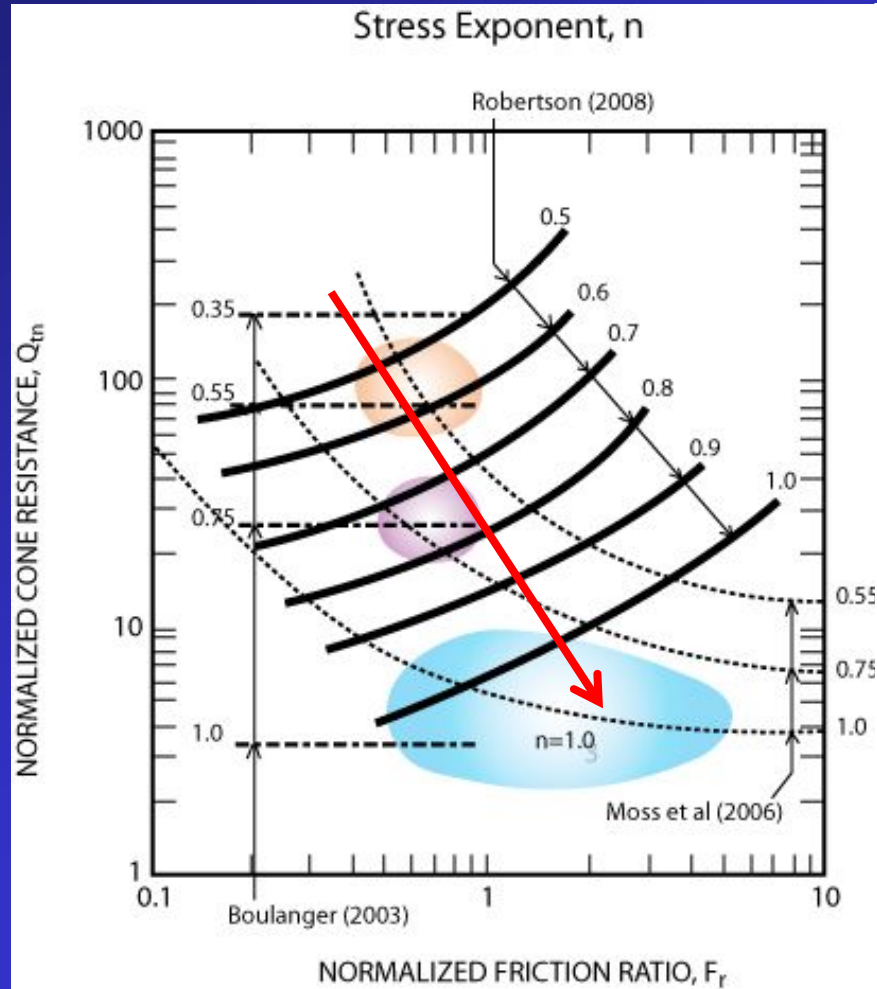
$$Q_{tn} = [(q_t - \sigma_v)/p_a] (p_a/\sigma'_{vo})^n$$

$$n = 0.381 (I_c) + 0.05 (\sigma'_{vo}/p_a) - 0.15$$

where $n \leq 1.0$

If stress normalization correct - no need
for additional stress level corrections
(e.g. K_s)

Compare stress normalization



Example CPT - UBC Fraser River

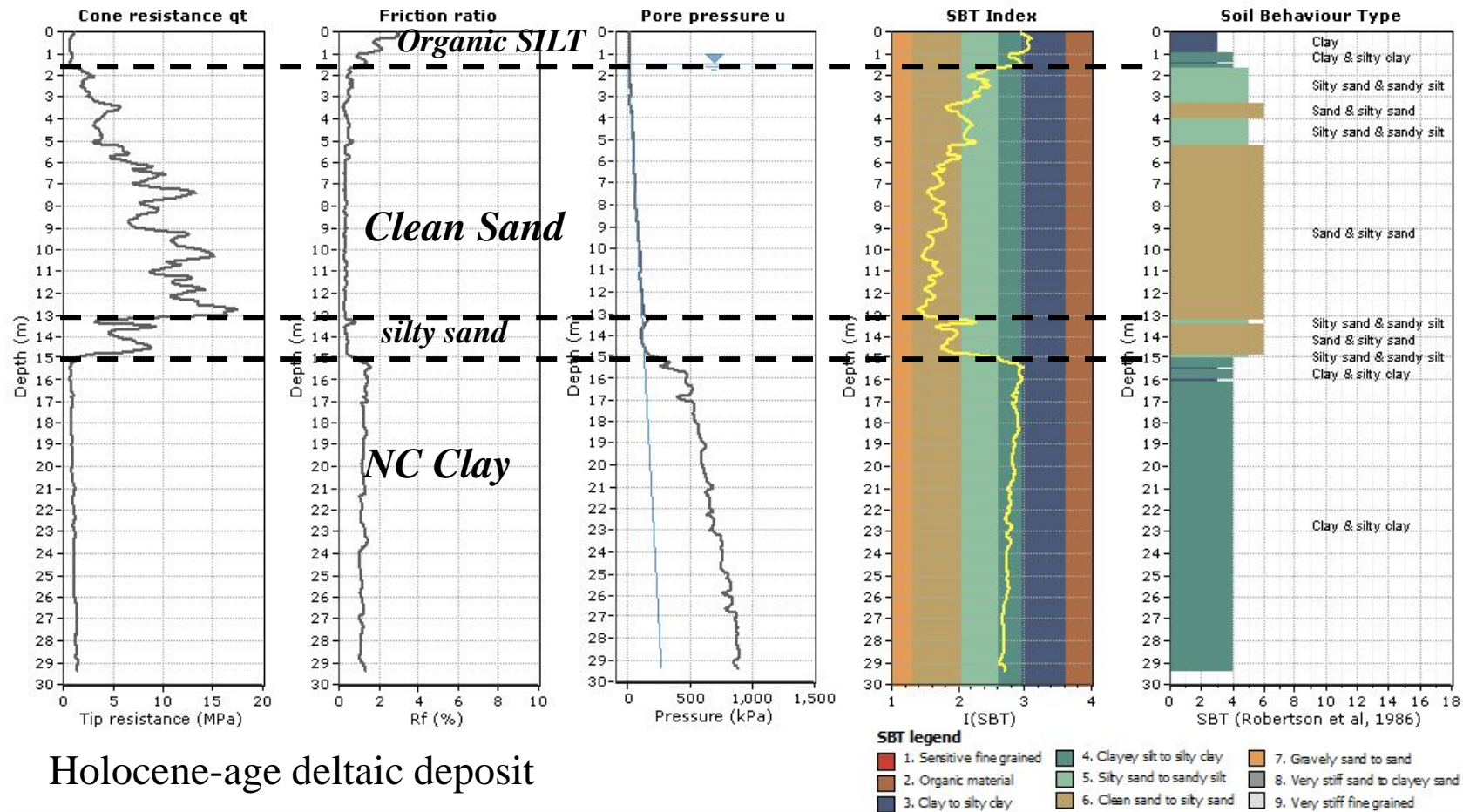


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Fraser River Delta, Vancouver, BC (UBC)
Campanella & Robertson, 1983

Project: UBC McDonalds Farm
Location: Vancouver, Canada

CPT: UBC McD Farm, Canada
Total depth: 29.35 m



Holocene-age deltaic deposit

Example CPT - UBC Fraser River

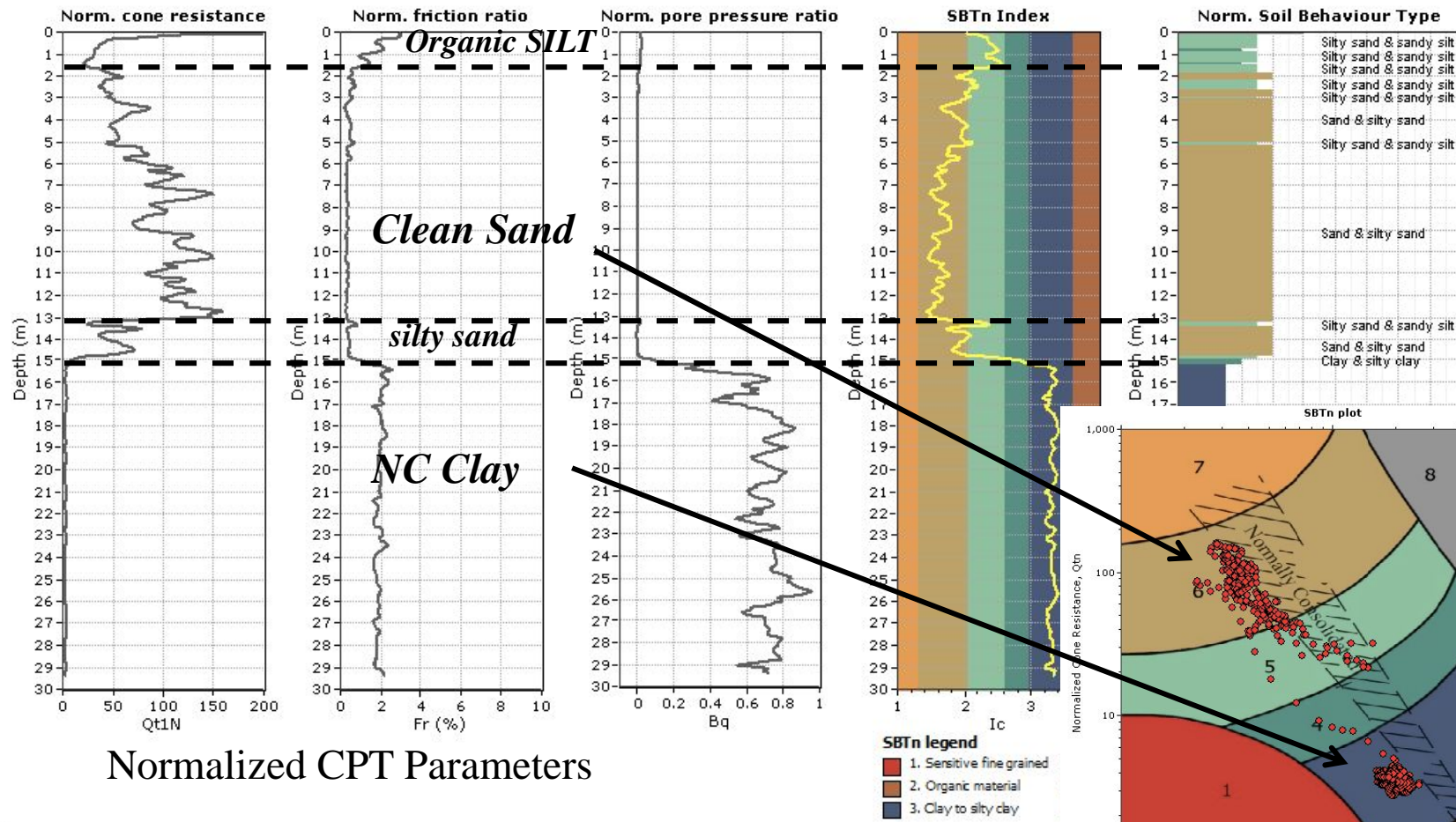


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Project: UBC McDonalds Farm
Location: Vancouver, Canada

Fraser River Delta, Vancouver, BC (UBC)
Campanella & Robertson, 1983

CPT: UBC McD Farm, Canada
Total depth: 29.35 m, Date: 12/4/2012



CPeT-IT v. 1.7.5.8 - CPTU data presentation & interpretation software - Report created on: 12/11/2012, 2:21:18 PM
Project file: Z:\Documents\Peter\Software\CPeT-IT\CPT Database\Mixed soil sites\Mixed soil sites.cpt

Example CPT – Venice Lagoon

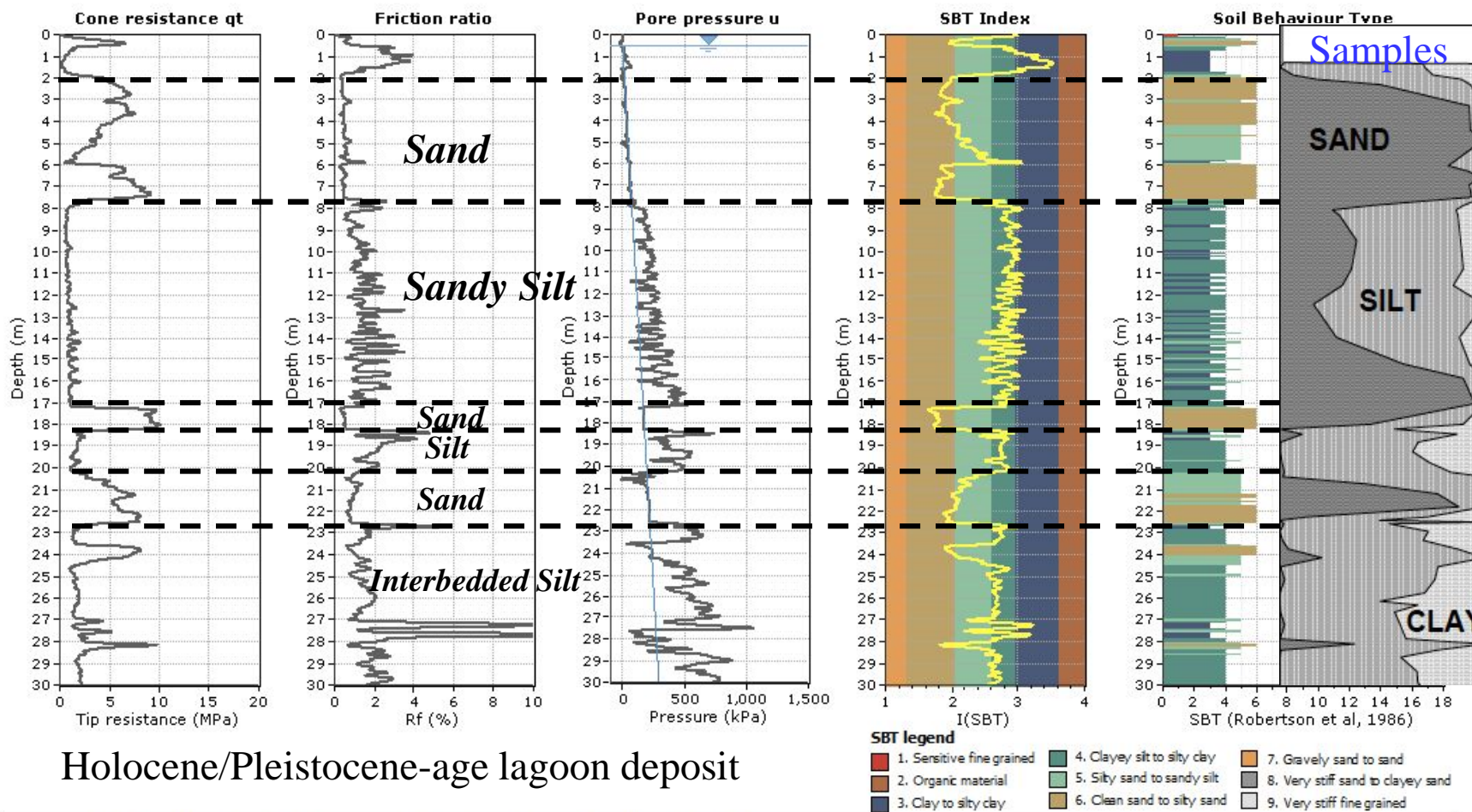


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Venice Lagoon, Treporti Test Site
Simonini et al, 2003

Project: Venice Lagoon, Italy
Location: Venice, Italy

CPT: Venice lagoon, Italy
Total depth: 45.67 m



Holocene/Pleistocene-age lagoon deposit

Example CPT – Venice Lagoon

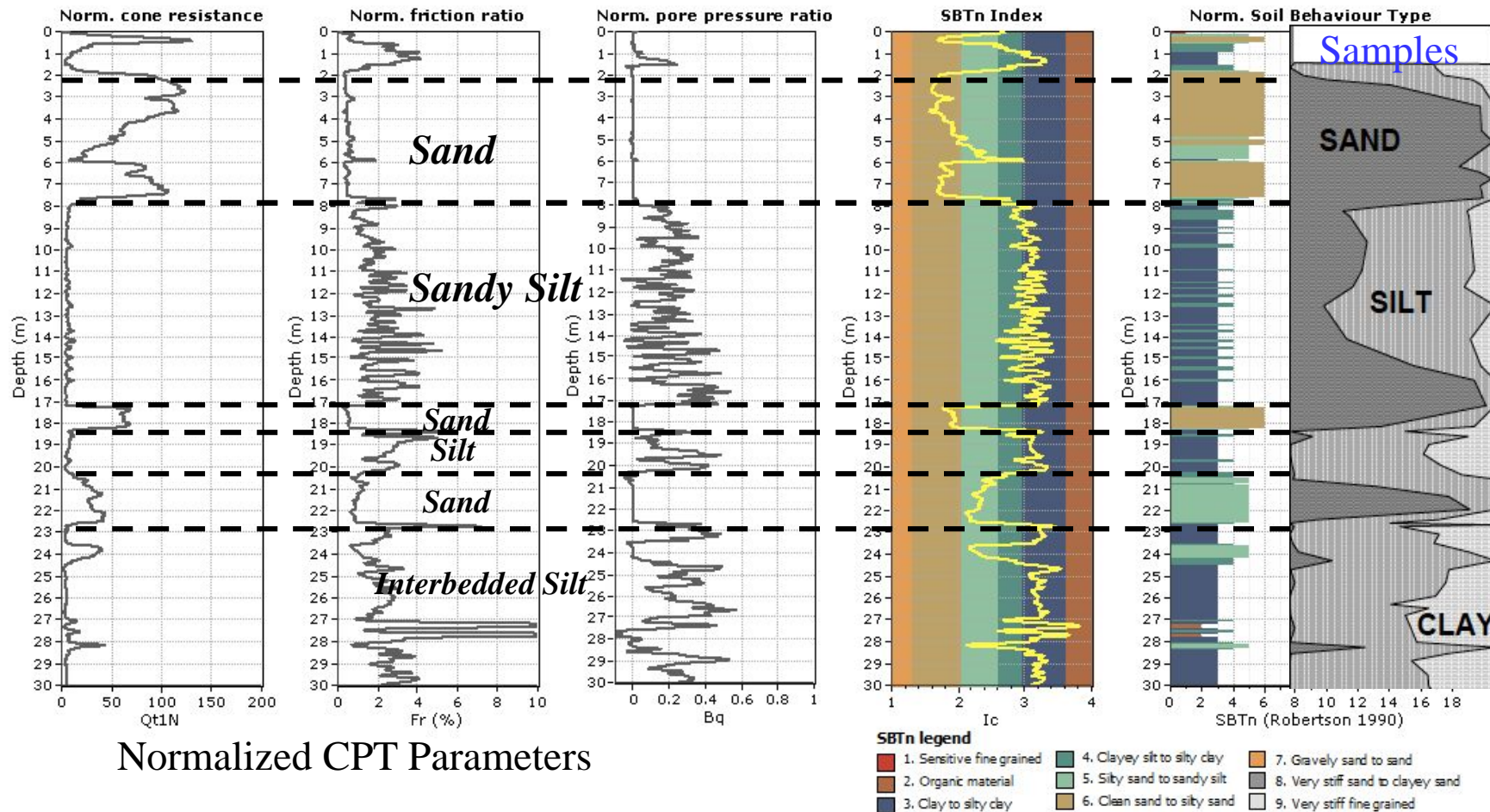


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Venice Lagoon, Treporti Test Site
Simonini et al, 2003

Project: Venice Lagoon, Italy
Location: Venice, Italy

CPT: Venice lagoon, Italy
Total depth: 45.67 m, Date: 11/27/2012



Normalized CPT Parameters

Example CPT

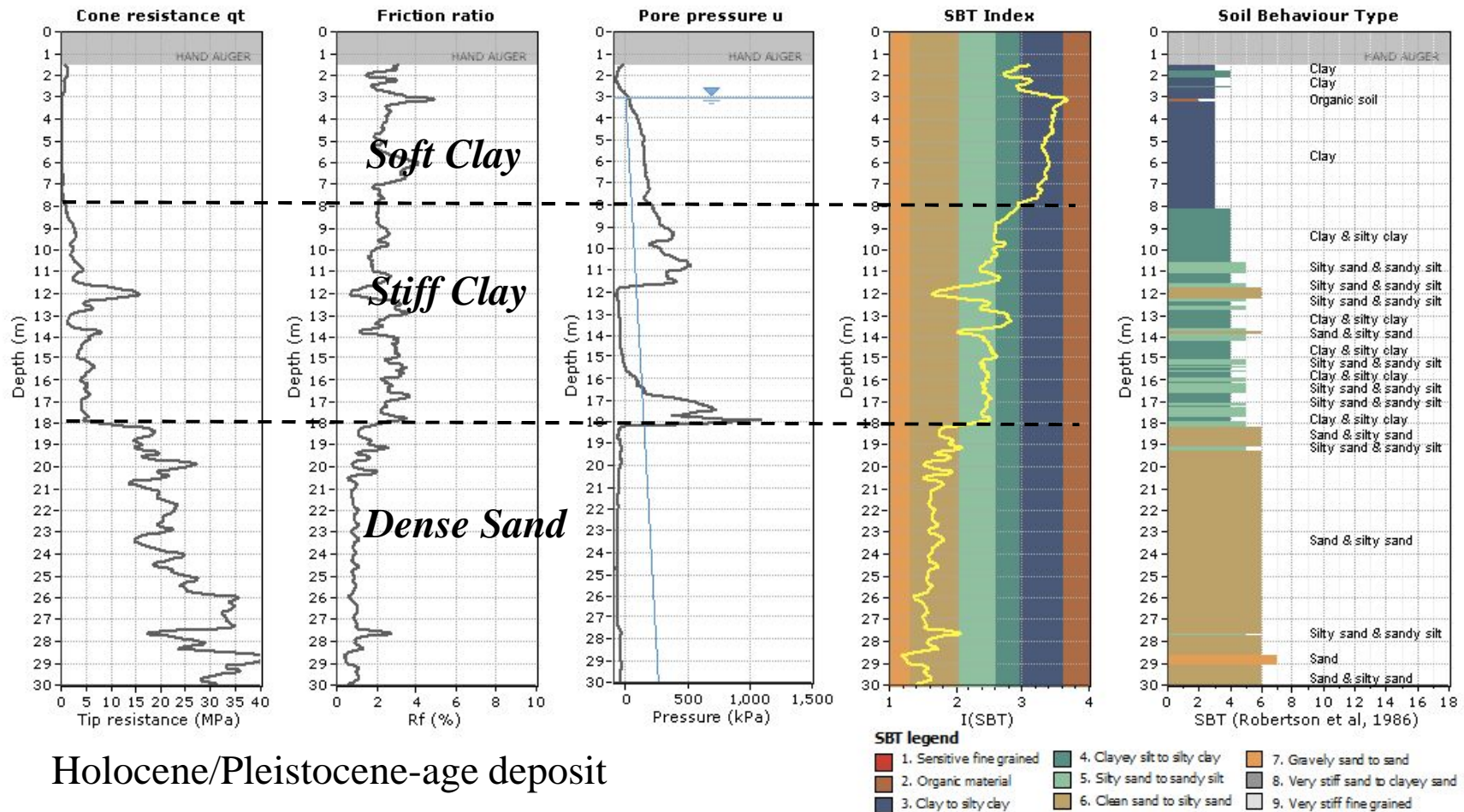


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Project: Example CPT
Location: California

Mixed soil profile
San Francisco Bay area, USA

CPT: CPT 1
Total depth: 30.50 m



Holocene/Pleistocene-age deposit

Example CPT



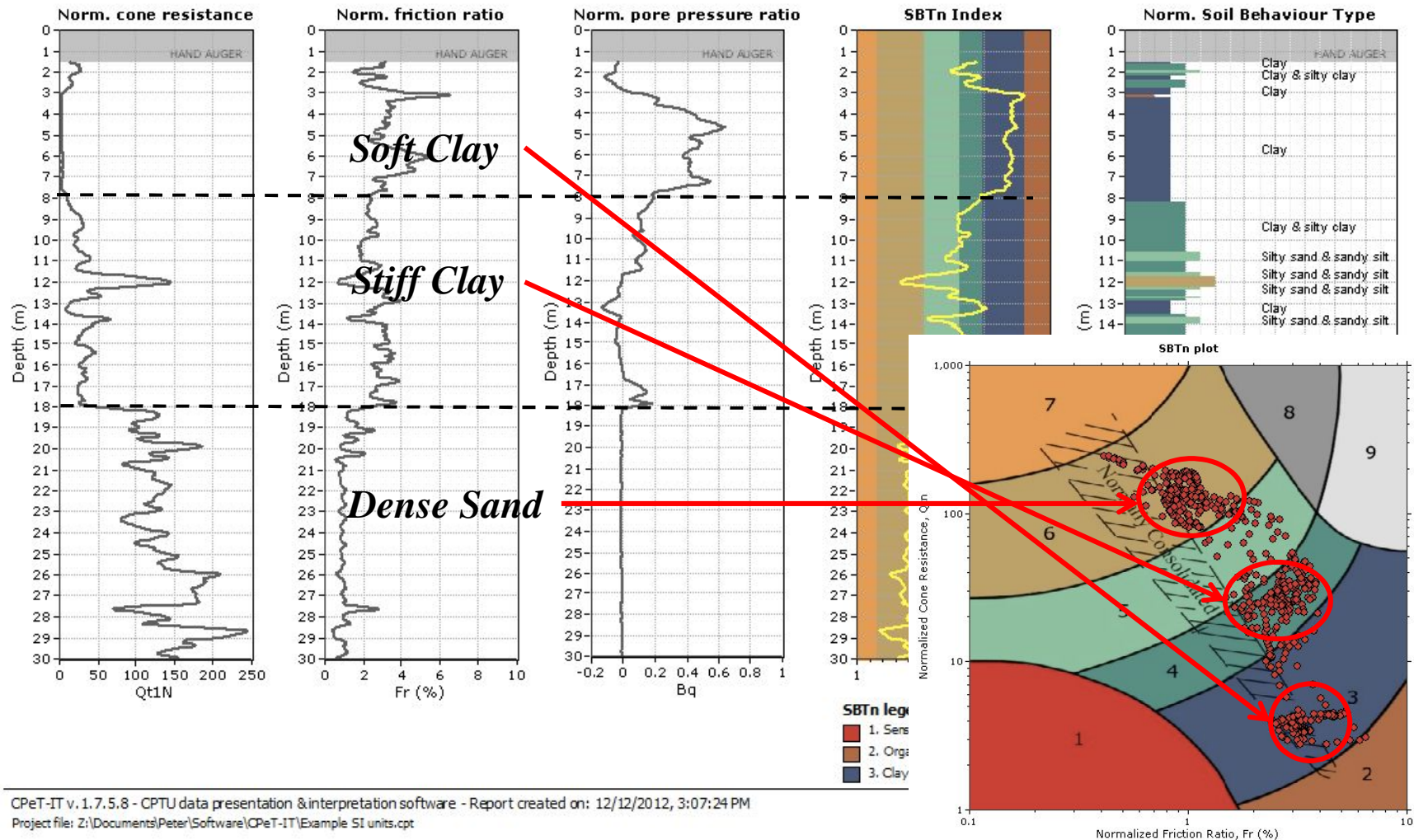
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Project: Example CPT
Location: California

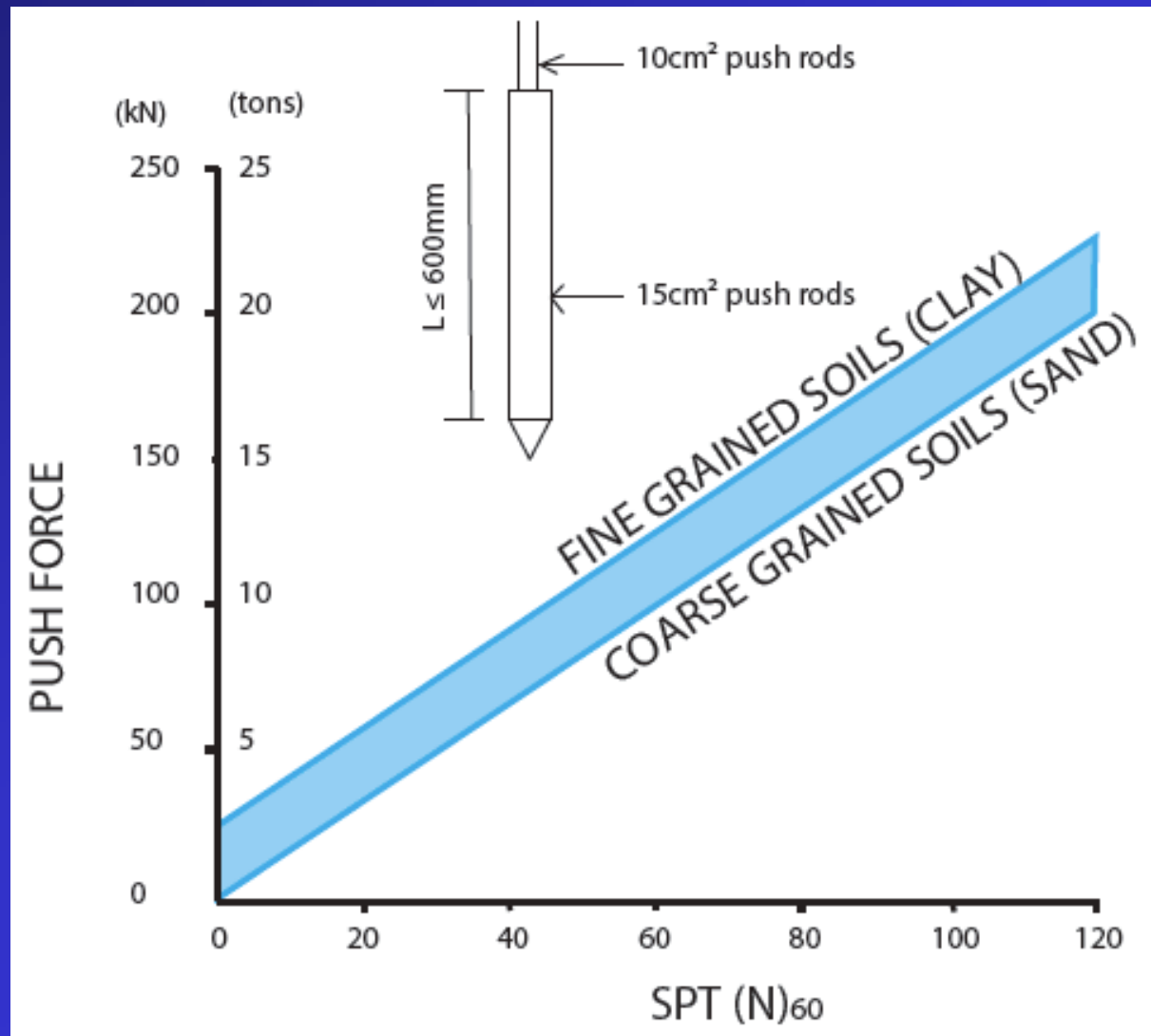
Mixed soil profile
San Francisco Bay area, USA

CPT: CPT 1

Total depth: 30.50 m, Date: 12/12/2012



How deep can you push the CPT?



Depends on:

- 1 - amount of reaction push force
- 2 - amount of rod friction

With 15 cm² cone (10cm² push rods) and 200 kN (20 tons) reaction – can penetrate soil with $SPT (N)_{60} > 100$

Example CPT – Mine Tailings

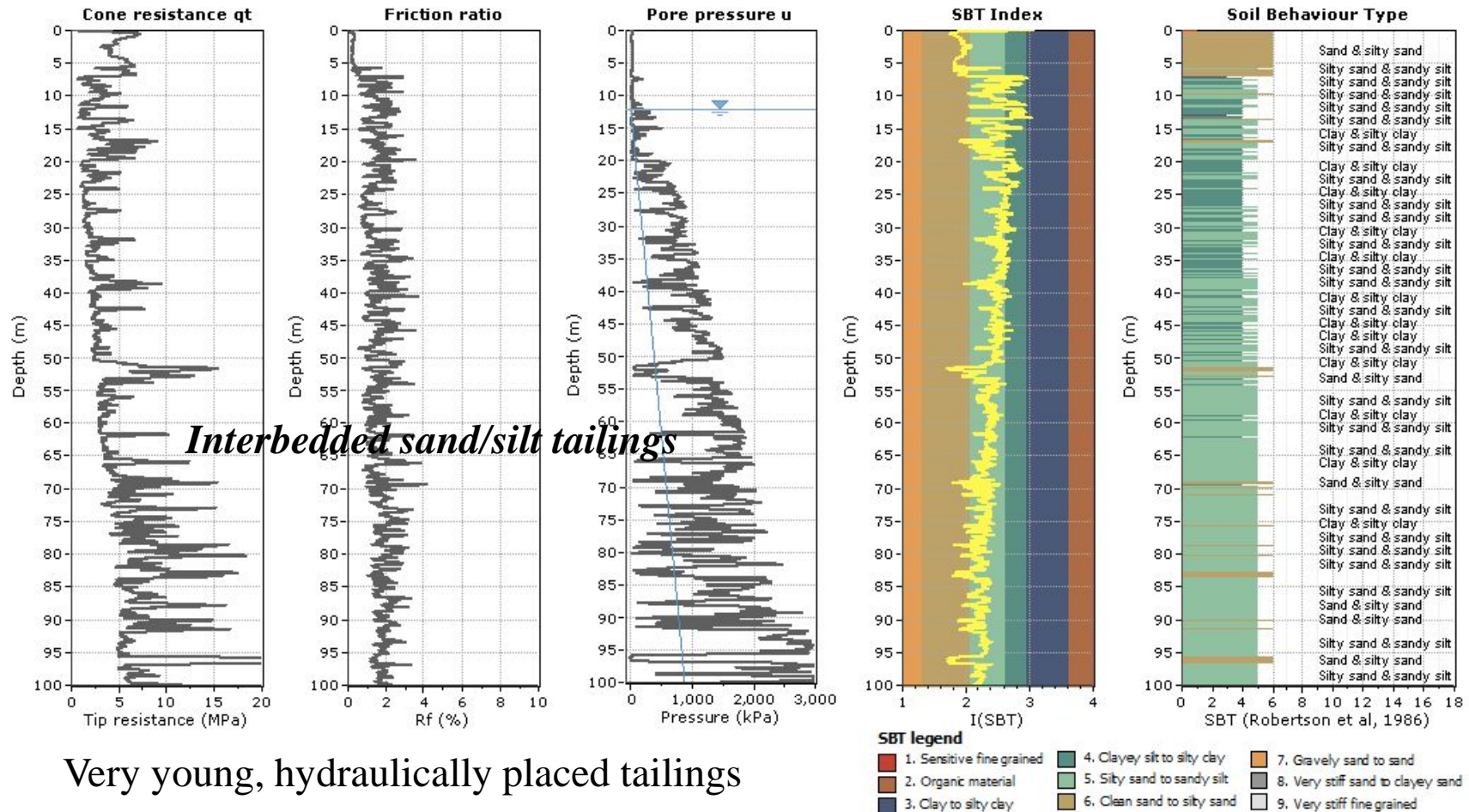


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Project: Mine Tailings Example
Location: USA

Deep Mine Tailings Southwest, USA

CPT: Mine Tailings
Total depth: 101.05 m



Very young, hydraulically placed tailings

Example CPT – Mine Tailings



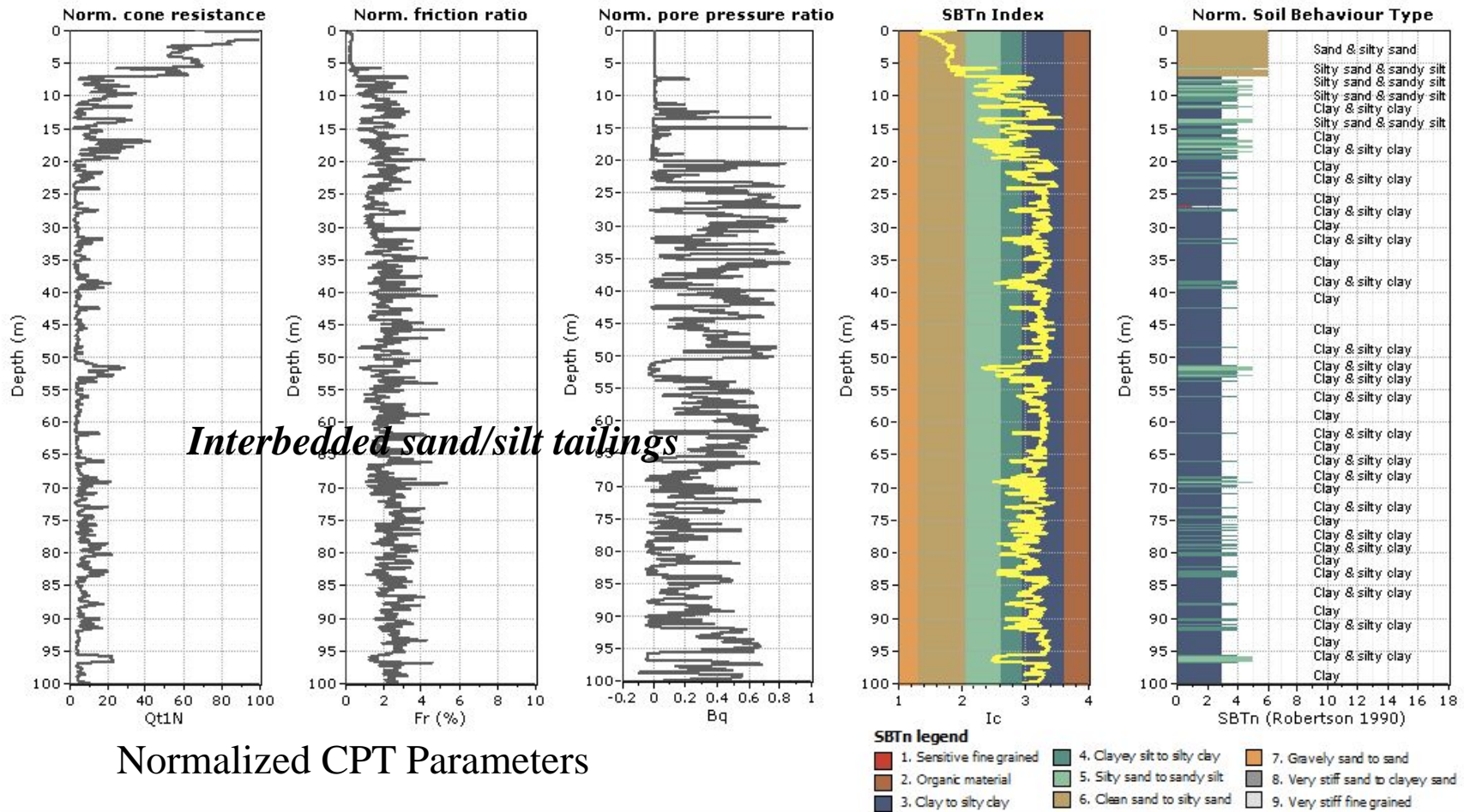
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Project: Mine Tailings Example
Location: USA

Deep Mine Tailings Southwest, USA

CPT: Mine Tailings

Total depth: 101.05 m, Date: 8/9/2012



Normalized CPT Parameters

Example CPT – Soft Rock

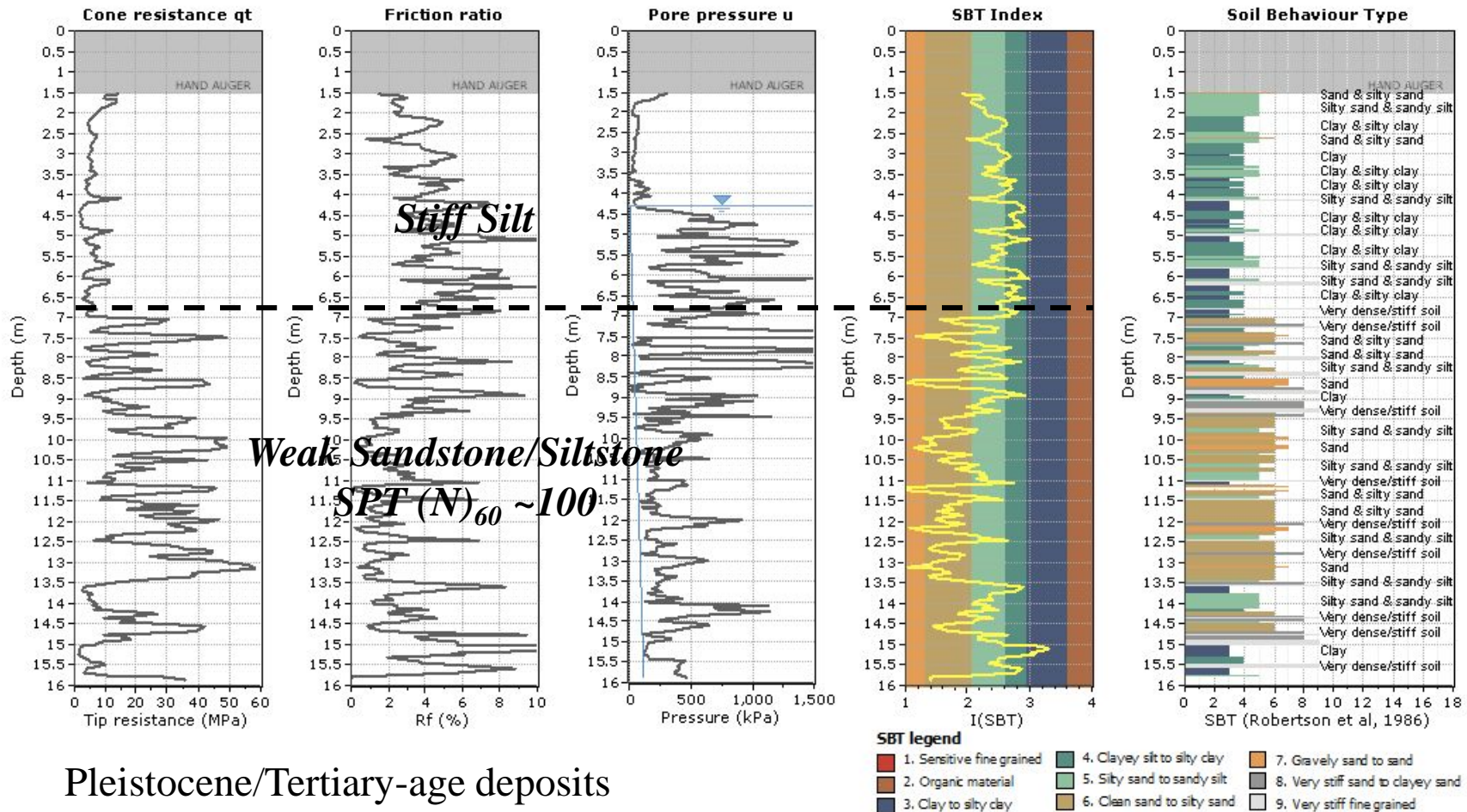


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Project: Stiff soil - soft rock
Location: Newport Beach, CA, USA

Very stiff soil – soft rock
Newport Beach, CA, USA

CPT: Newport Beach, CA
Total depth: 15.85 m



Pleistocene/Tertiary-age deposits

Example CPT – Soft Rock

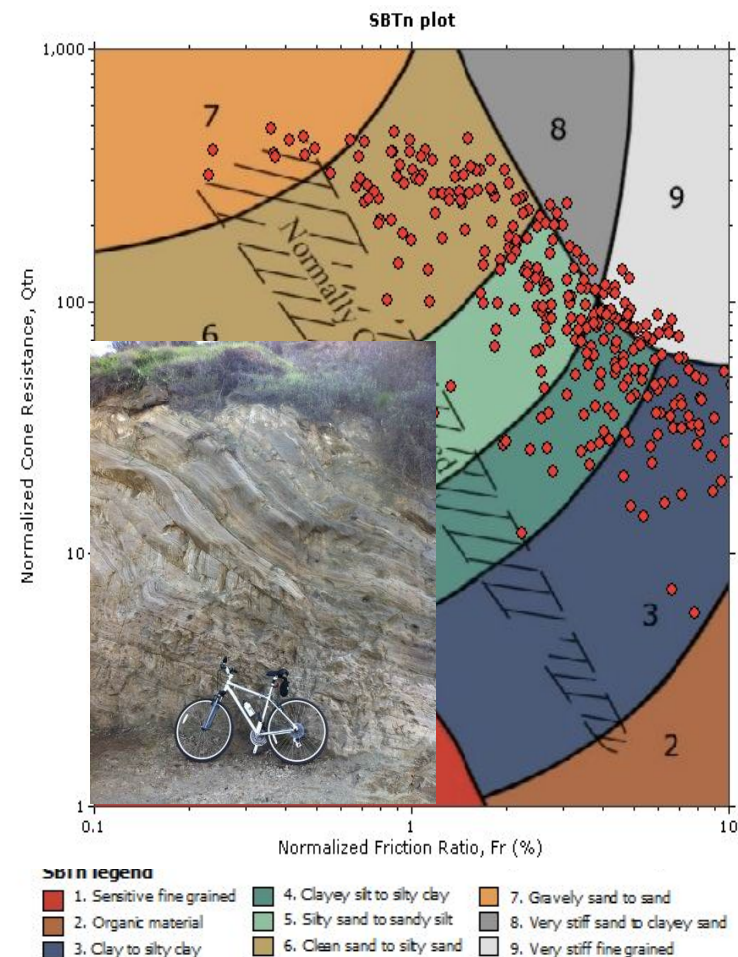
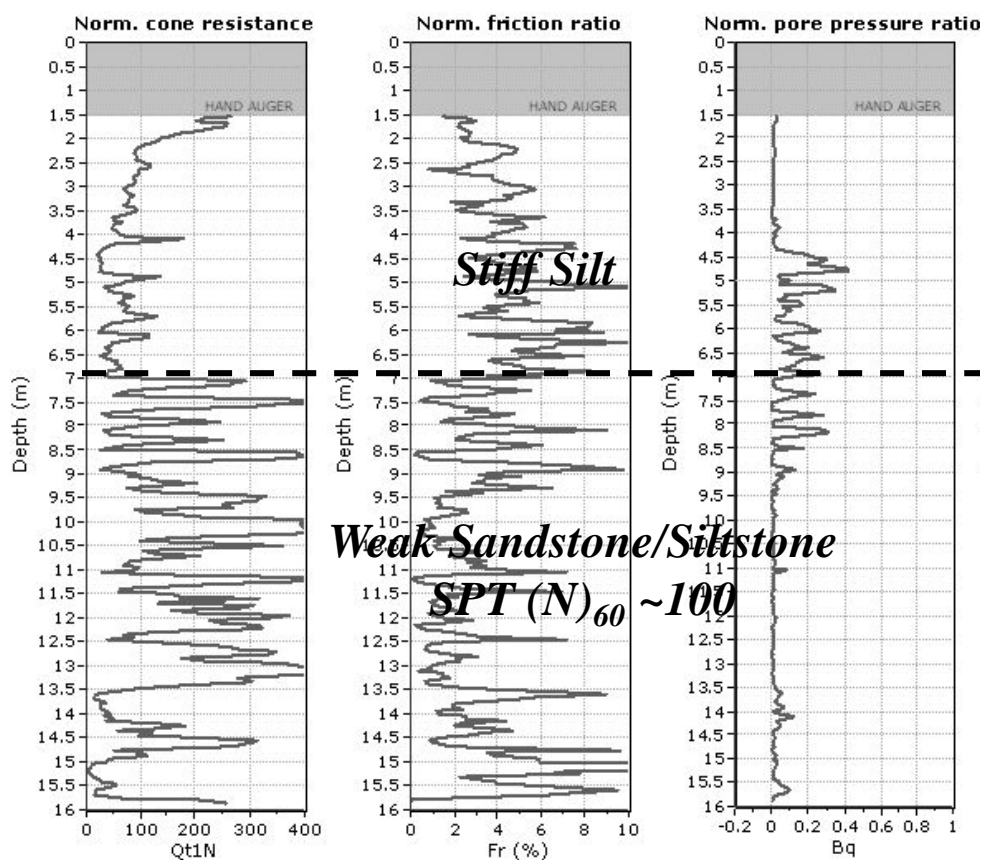


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Gregg Drilling & Testing Inc
www.greggdrilling.com

Project: Stiff soil - soft rock
Location: Newport Beach, CA, USA

Very stiff soil – soft rock
Newport Beach, CA, USA

CPT: Newport Beach, CA
Total depth: 15.85 m, Date: 12/12/2012



Normalized CPT Parameters

Summary

- CPT is a fast, reliable method to determine soil stratigraphy and soil type in a cost effective manner.
- CPT-based Soil Behaviour Type (SBT) charts available to estimate soil type, based on either tip-friction and/or tip-pore pressure measurements
- CPT equipment can be used to take small diameter push-in soil samples to verify soil type